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cicli**

**Torino, November 5, 2008**

# **Fatigue Crack Initiation, Propagation and Failure at Very-High Numbers of Cycles**

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**BOKU University of Natural Resources and Applied Life Sciences  
Vienna, Austria**

# Contents

- **Very high cycle fatigue (VHCF), fatigue crack growth (FCG) and  $\Delta K$  thresholds at ultrasonic frequency**

Experimental procedure and results:

S-N and ( $\Delta a/\Delta N - \Delta K$ ) curves of **different materials**

Influence of environment and frequency

- **Plastic deformation, crack initiation, propagation and failure in **copper** in the VHCF range (20 kHz)**

Persistent slip bands (PSBs)

Endurance limit ,  $\Delta a/\Delta N$  and  $\Delta K$  threshold

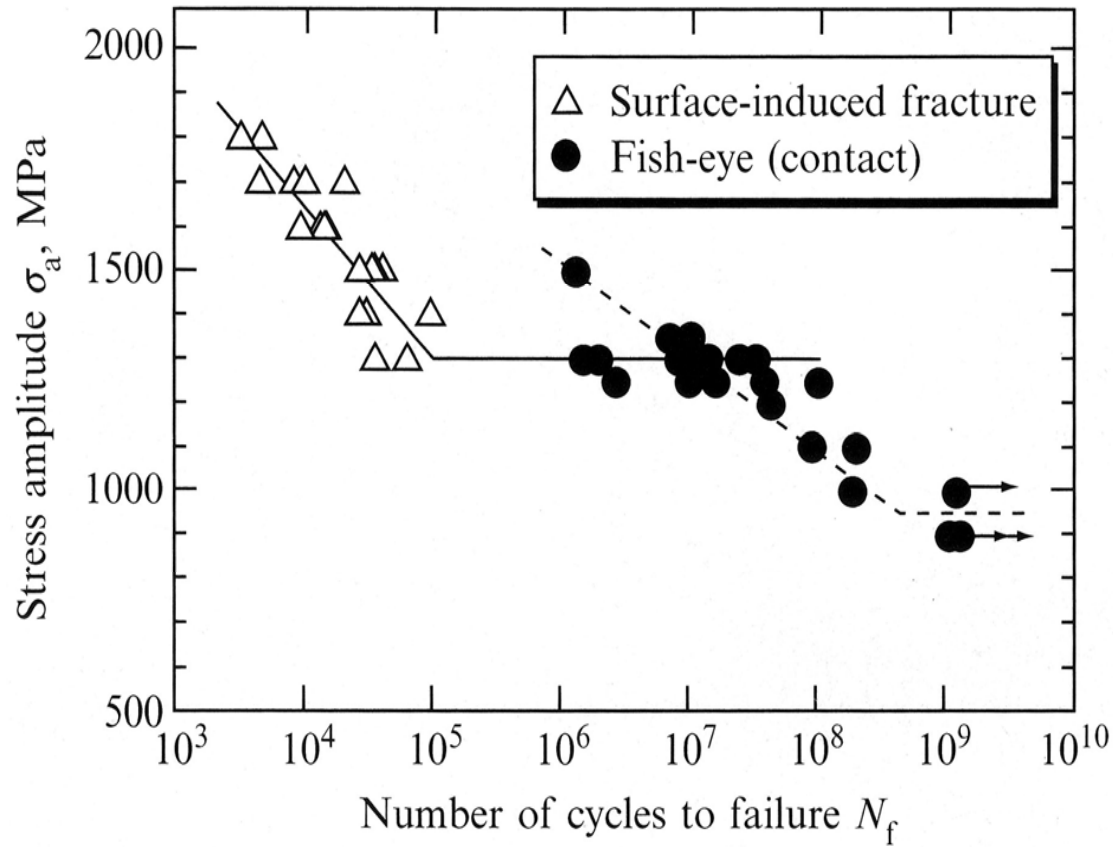


*Torino*  
*5 novembre 2008*

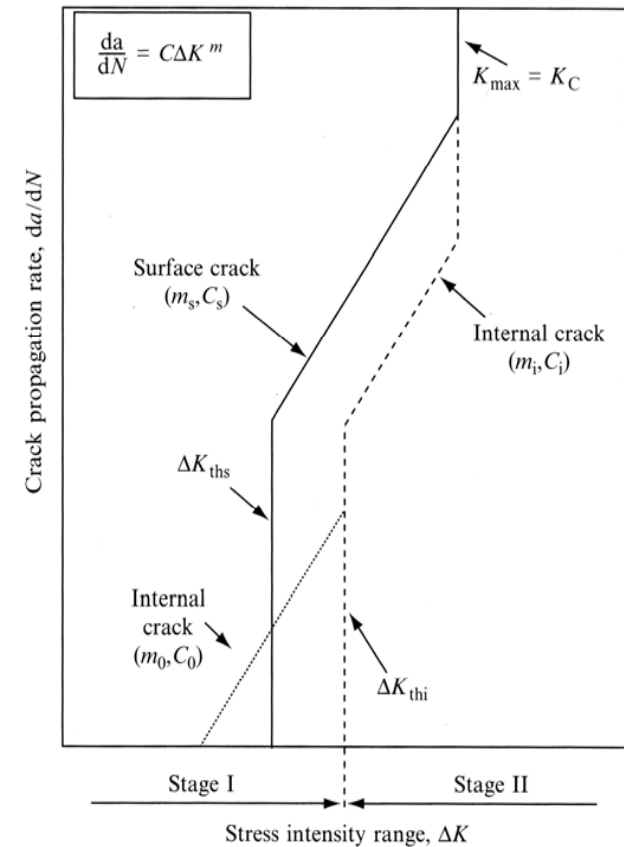
*Stefanie Stanzl-Tschegg*



# VHCF and FCG Behaviour

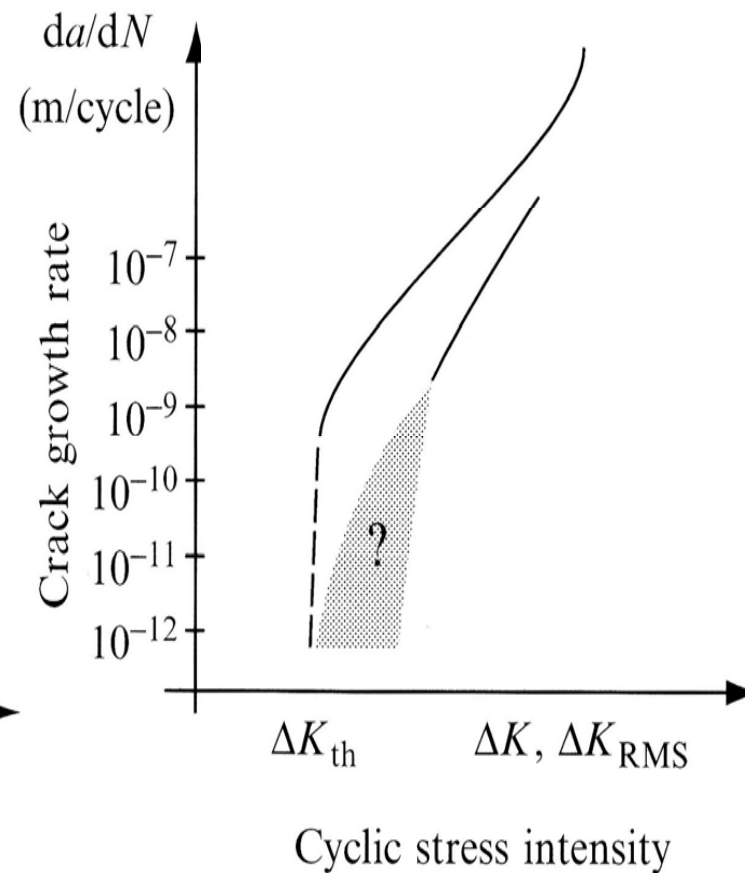
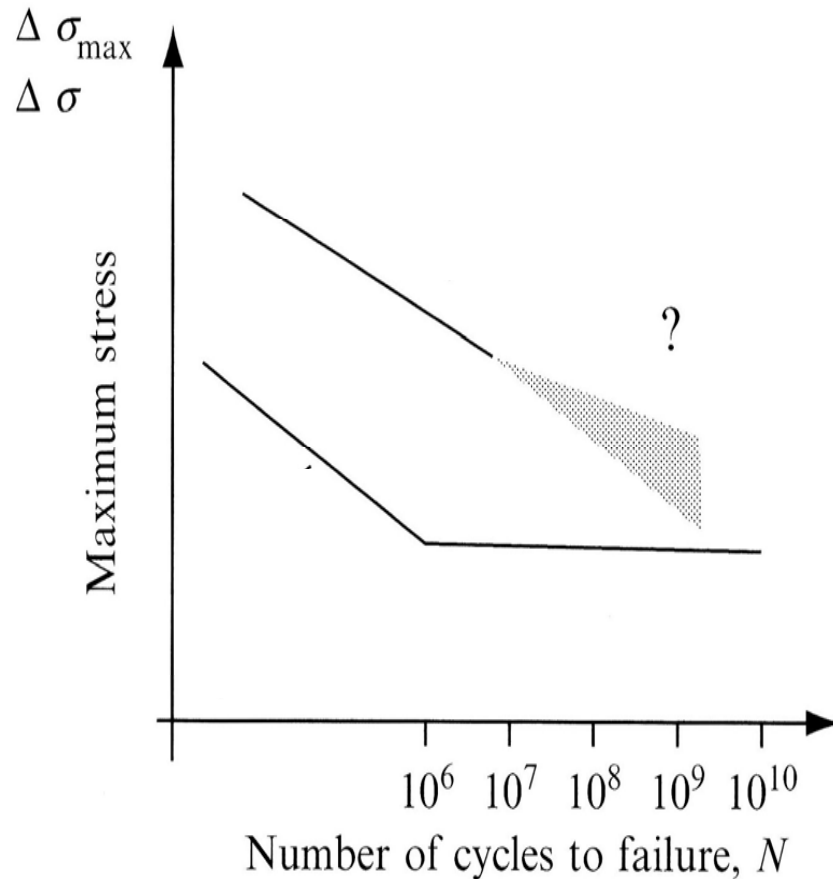


S-N diagram of high-carbon Cr-steel (Sakai et al 2002)



FCG behaviour of Surface and internal cracks (Tanaka & Akiniwa 2002)

# Existence or Non-Existence of Endurance Limit and Threshold Stress Intensity



# VHCF – Testing Times

Number of cycles	20 Hz	20 kHz
$10^6$	14 hours	50 sec
$10^7$	6 days	8 min
$10^8$	2 months	1.4 hours
$10^9$	1.7 years	14 hours
$10^{10}$	17 years	6 days
$10^{11}$	170 years	2 months



*BOKU University  
1915*

# Ultrasound Measuring Technique



*BOKU University  
2004*

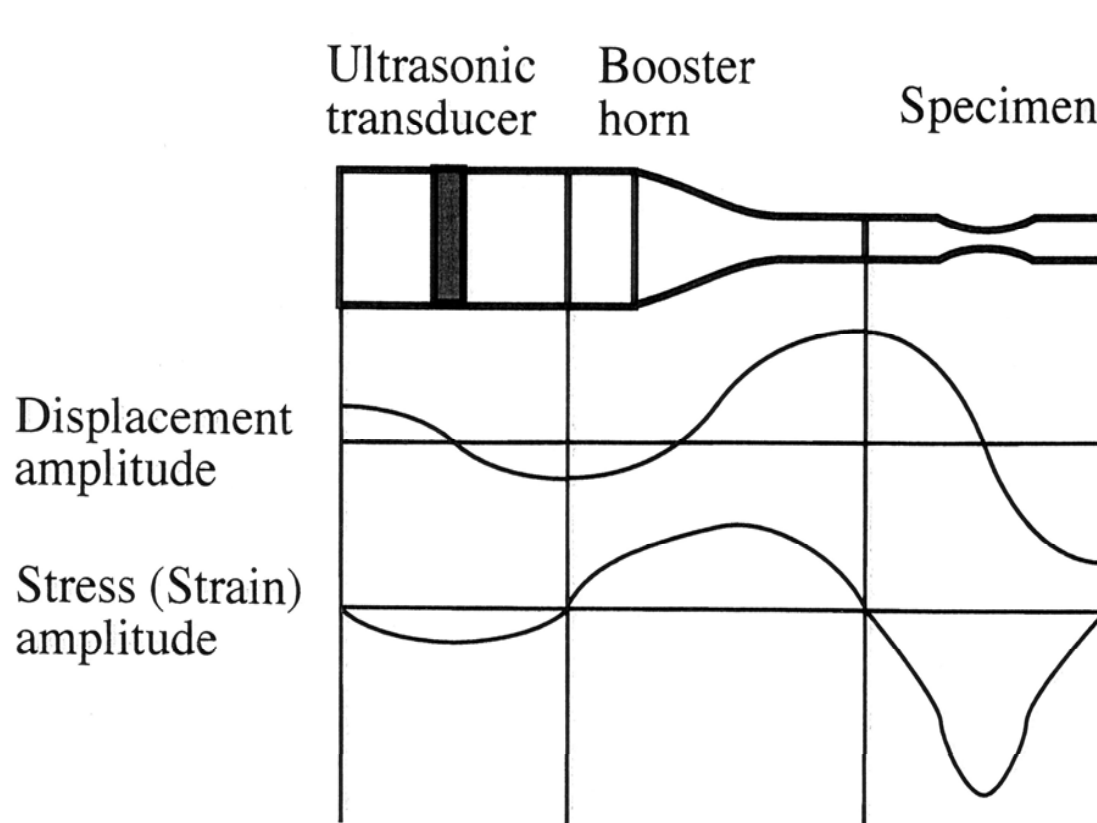


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5 novembre 2008*

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# Principle of Ultrasonic Resonance Fatigue Loading



Resonance vibration at approximately 20 kHz

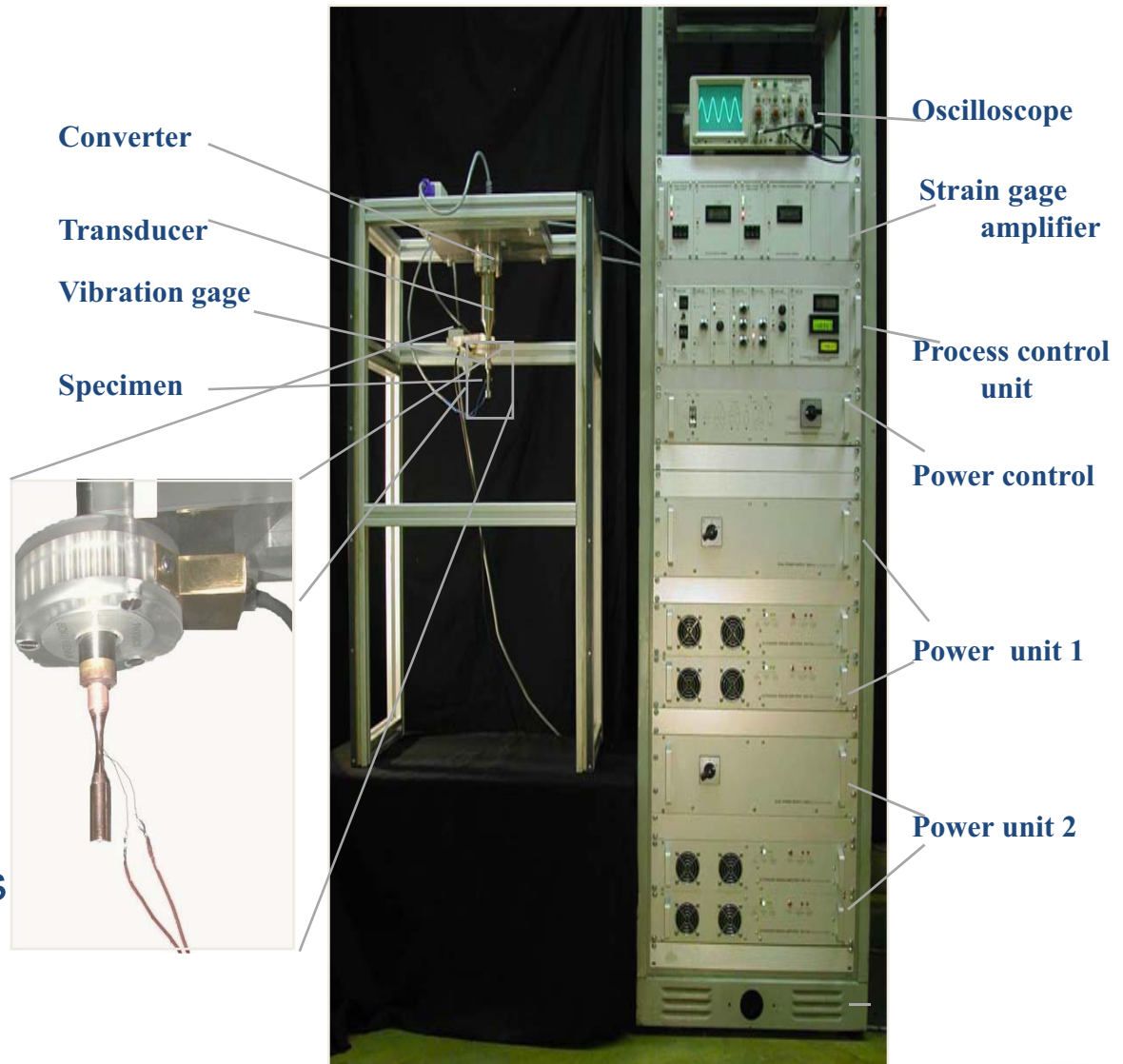
•**Ultrasonic Transducer:**  
Piezoelectric, axial or torsional

•**Magnification Horn:**  
Increases the vibration amplitude by a factor of 4 to 15

•**Specimen:**  
Length and shape follows resonance criteria,  
Surface condition is important  
Smooth or notched

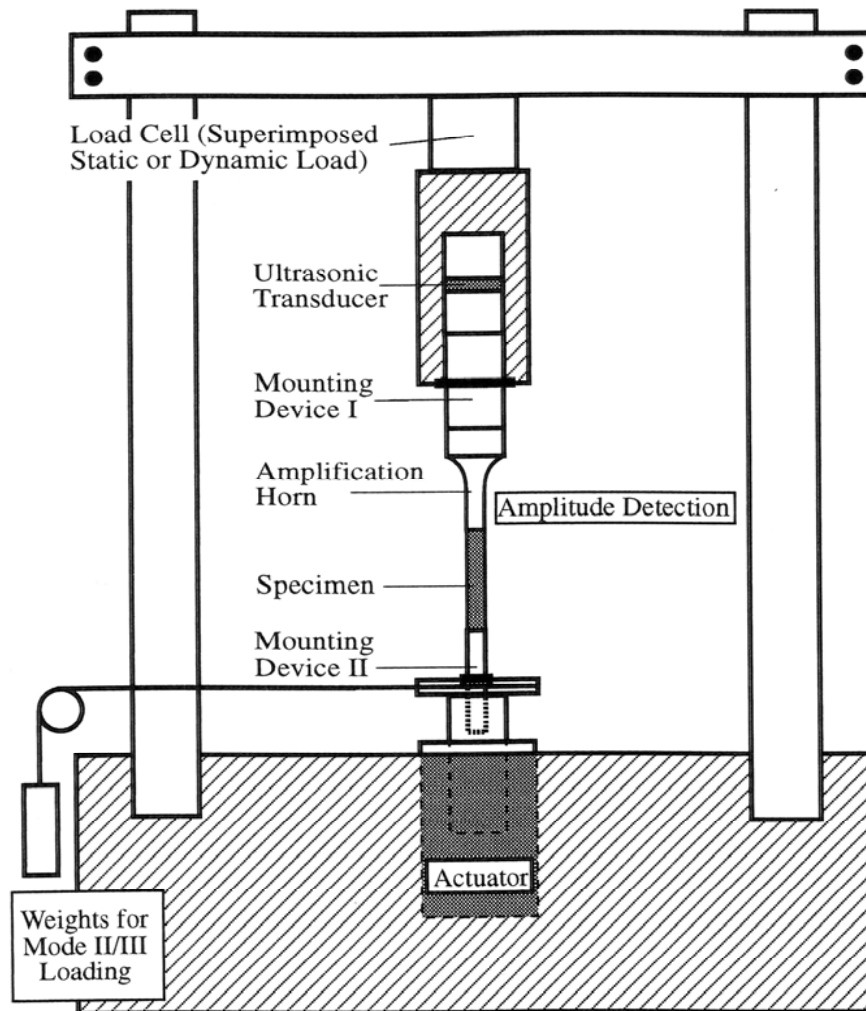
# Ultrasonic Fatigue Loading – Experimental Procedure

- **Frequency 19 kHz**
- **Fully reversed loading**  
( $R=-1$ )
- **Cooling (damping heat):**  
compressed air  
pulse-pause sequences  
pulses: 150 ms (2700 cycles)  
periodic pauses: 2000-3000 ms
- **Induction sensor**  
measures vibration  
amplitudes
- **Closed loop control**  
of vibration amplitudes  
(total strain)





# Ultrasound Testing Equipment



- Amplitude sensor

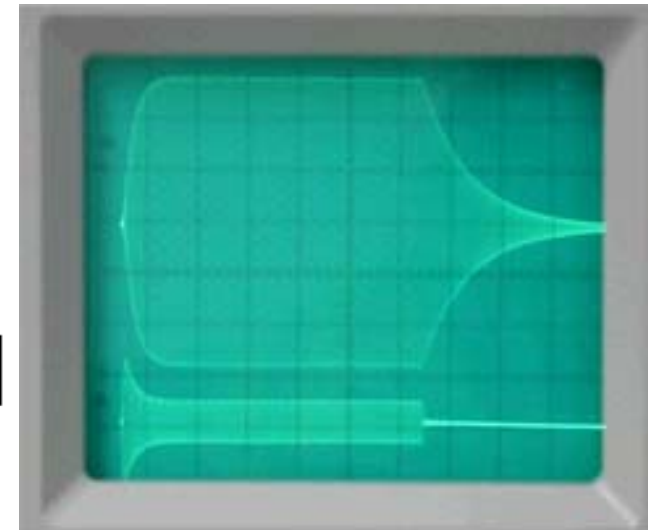
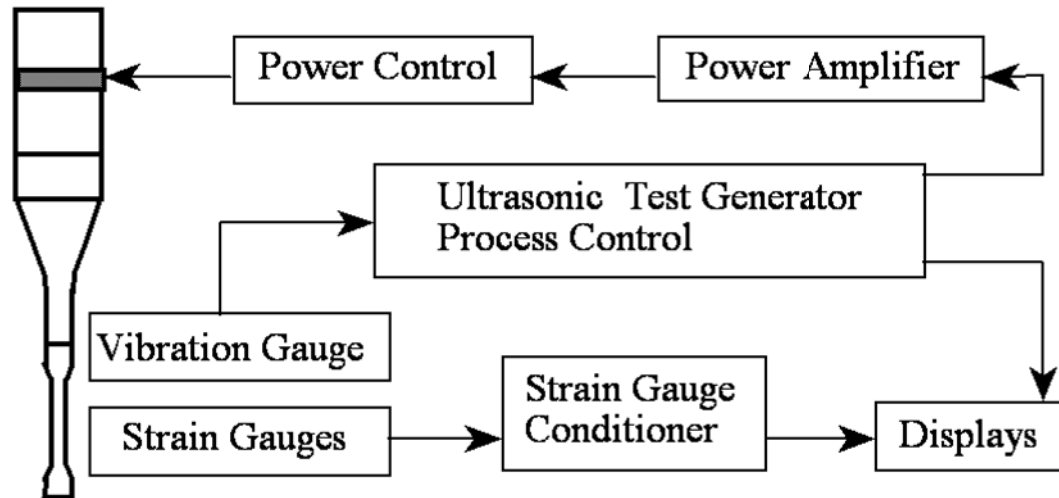
$$\Delta l \rightarrow \varepsilon = \Delta l / l \rightarrow$$

$$\sigma = E \cdot \varepsilon \rightarrow \Delta K$$

- Free specimen end  $\rightarrow R = -1$
- Both specimen ends fix  $\rightarrow R \geq 1$
- Cooling Pulse-Pause  
+ Compressed air
- Environmental chambers  
(corrosion, temperature, vacuum)

# Ultrasonic Testing Procedure

## Amplitude feed-back control



### Determination of the process:

**Vibration Amplitude:** After calibration

**Pulse and Pause:** Depending on damping

**Frequency limits:** Stop when specimen failure

### Control Circuits:

**Vibration Amplitude:** Accuracy  $\pm 1\%$

**Resonance Frequency:** Accuracy  $\pm 1$  Hz (0.005%)

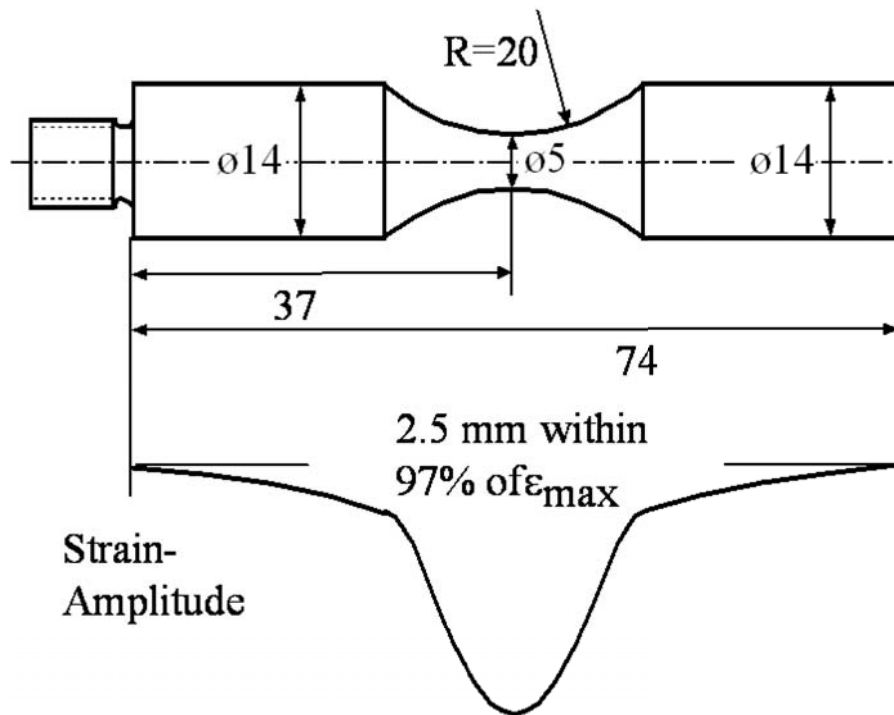
**Pulse 50 ms** - approx. 1000 amplitudes

**Increase Time** - approx. 100 amplitudes

**Decay Time** - depending on damping

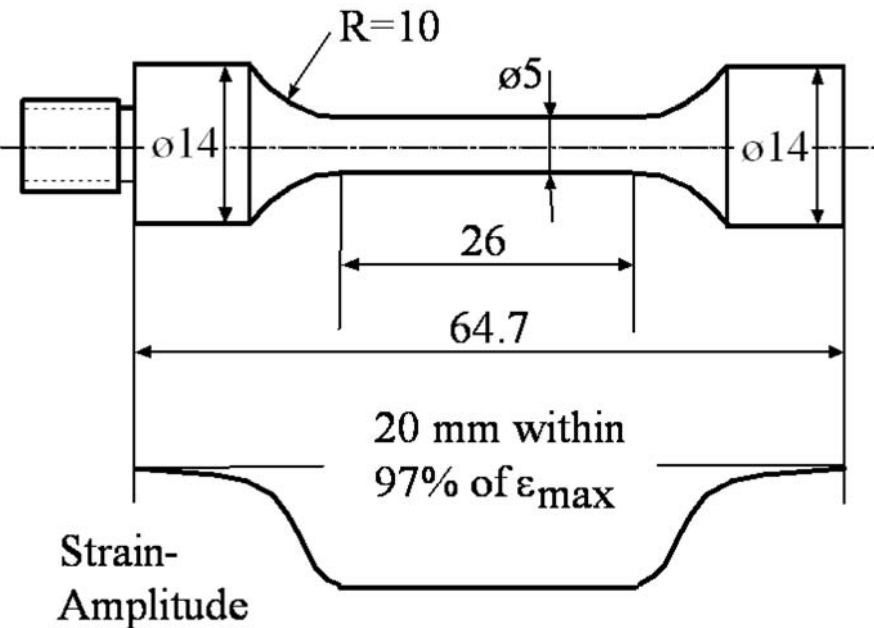
# Shapes of Fatigue Specimens

## Wrought alloy



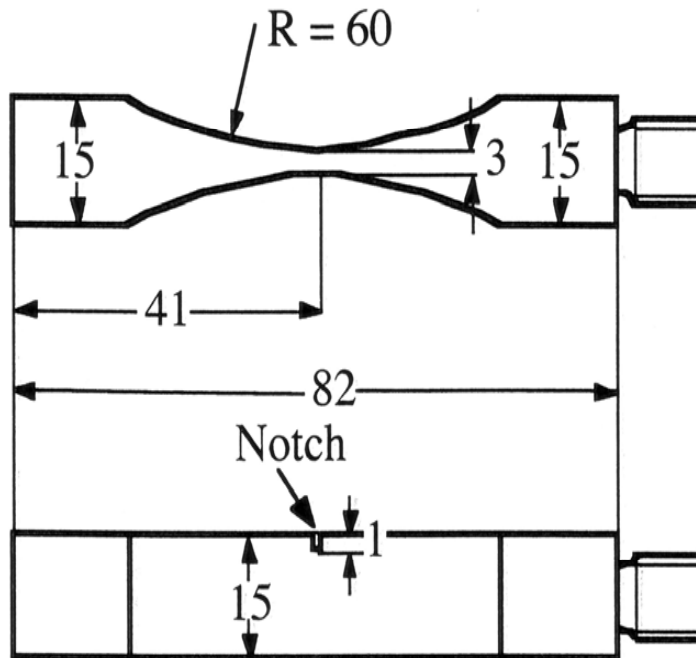
Amplification factor: 4.9  
Loaded volume: 50 mm<sup>3</sup>

## Cast alloy

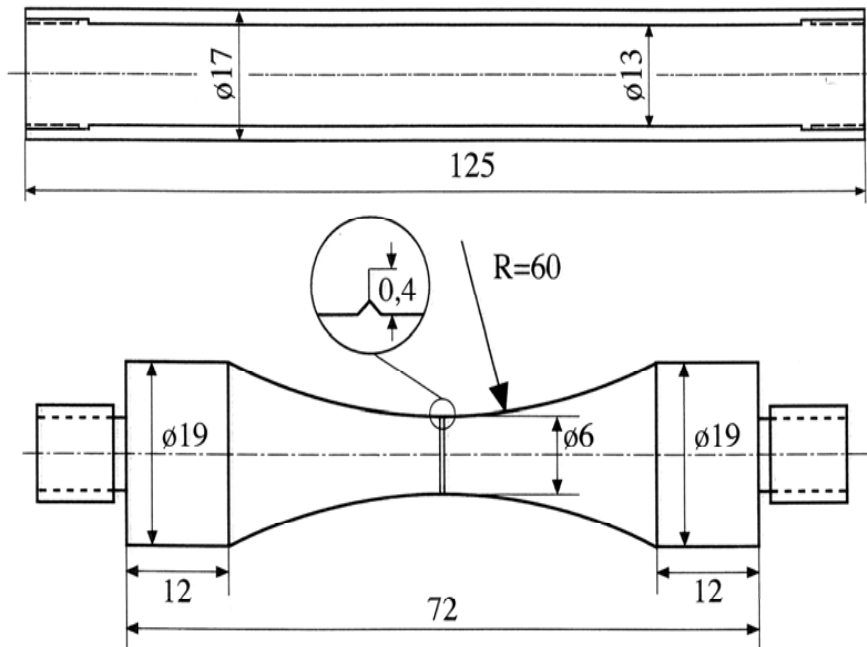


Amplification factor: 2.2  
Loaded volume: 390 mm<sup>3</sup>

# Specimen Shapes - Fatigue Crack Growth



Fully Reversed Loading



Superimposed and Mixed Mode Loading

# Ultrasonic Fatigue Testing Procedure – Mechanical Components

## Testing in different environments

Vacuum

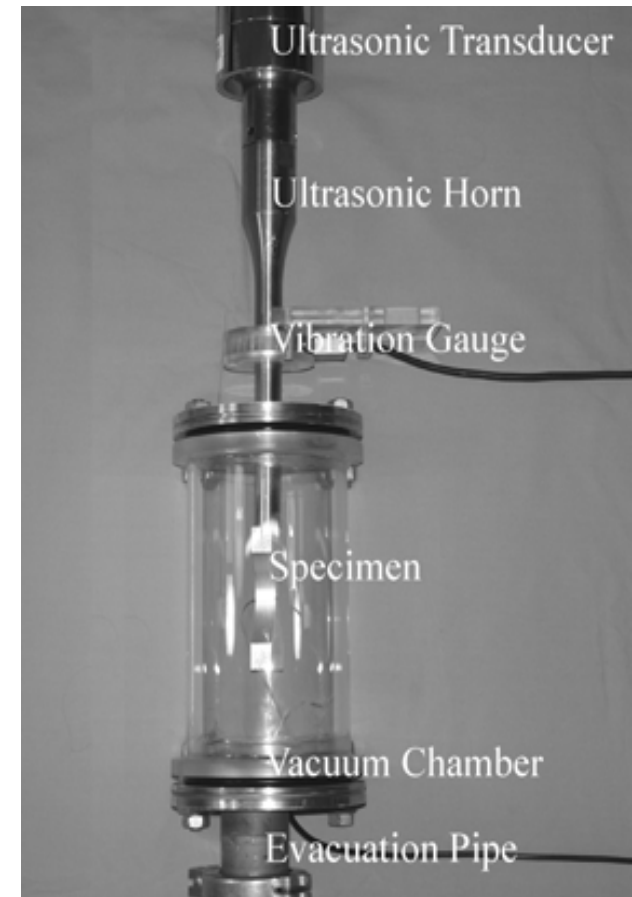
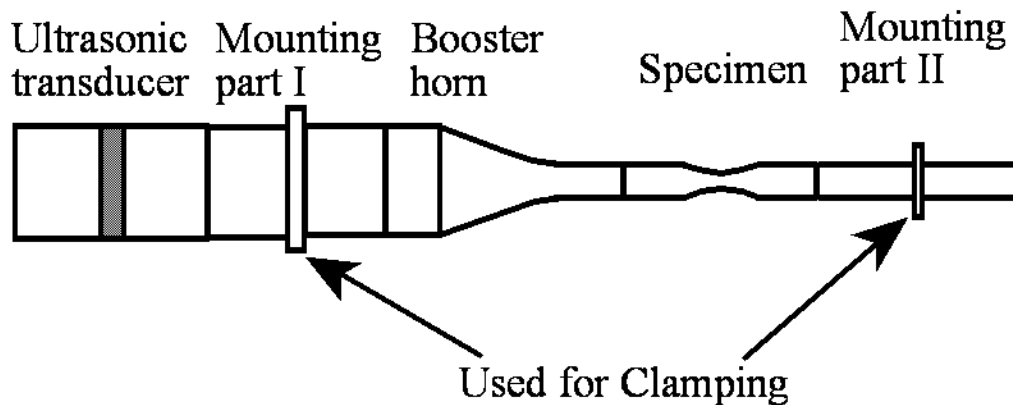
High and low temperature

Corrosive Fluids

## Testing at different loading conditions

Superimposed mean loads ( $R > -1$ )

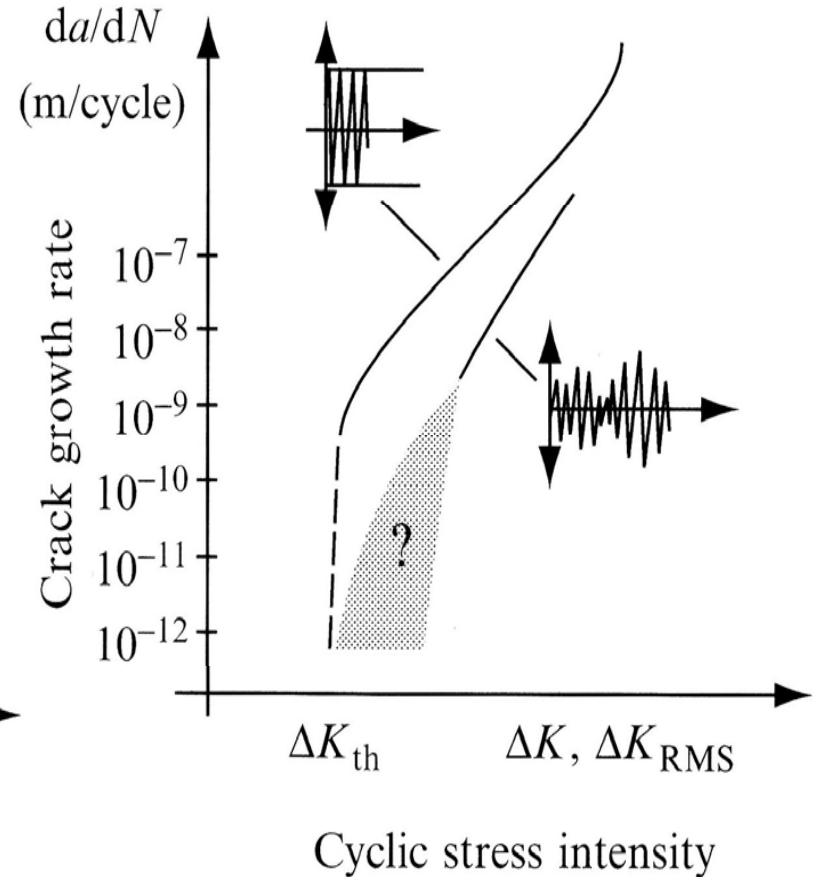
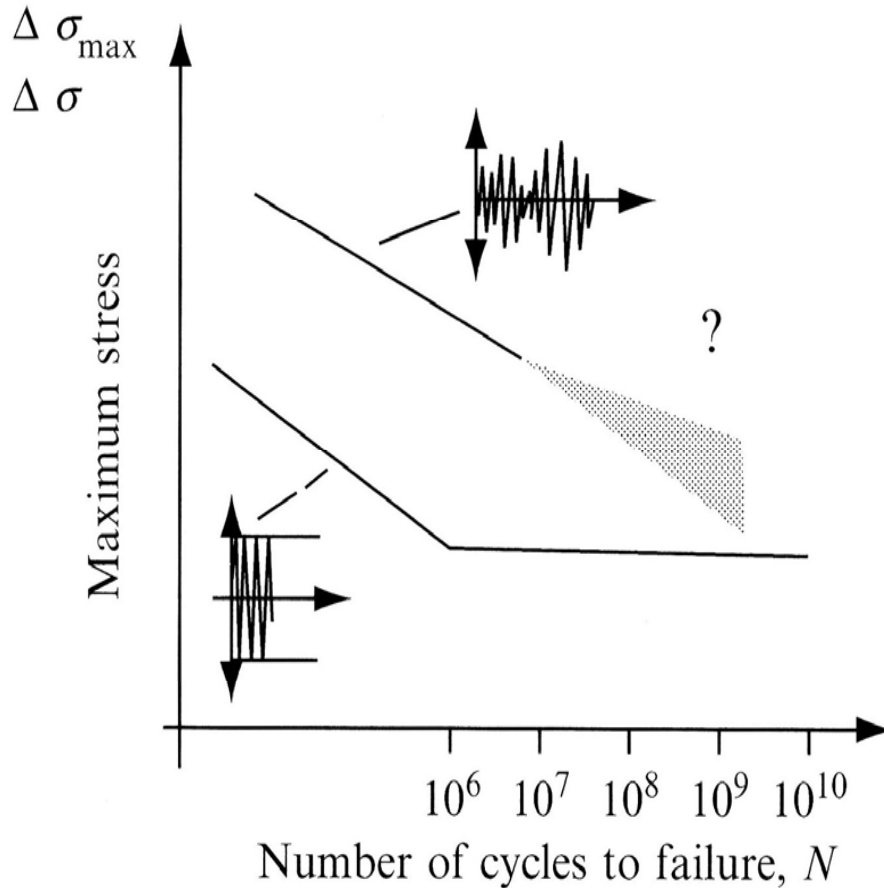
Superimposed torsion moments



*Testing in vacuum*

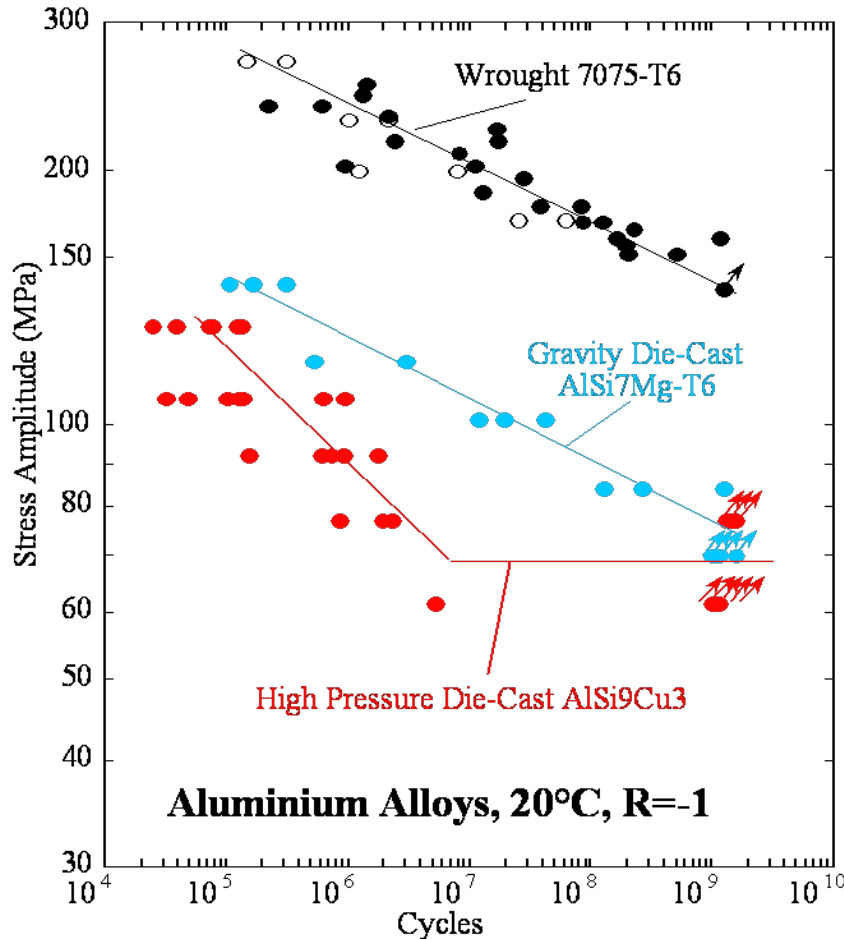
# Random loading

## Endurance Limit - Threshold Stress Intensity



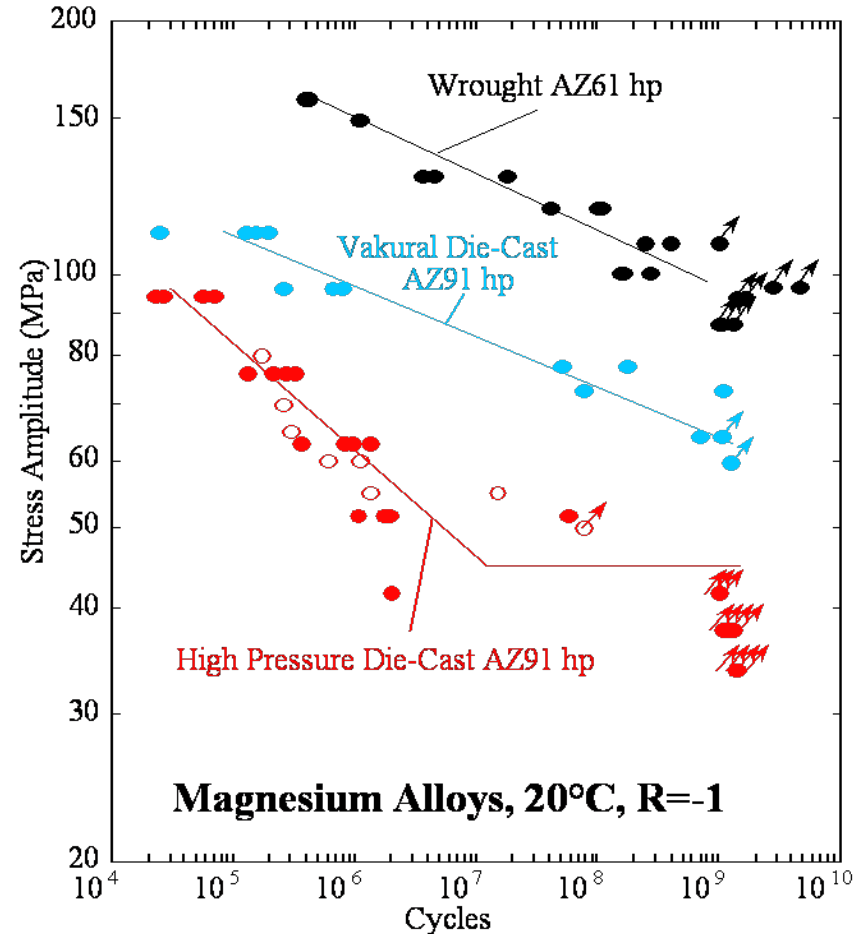
# VHCF Aluminium and Magnesium Alloys

## S-N Curves



Papakyriacou M, Mayer H, Fuchs U,  
Stanzl-Tschegg SE, FFEMS 25, 2002.

Stanzl-Tschegg SE, Proc.  
ATEM'93, 2003, 03-207



Mayer H, Papakyriacou M, Zettl B, Stanzl-  
Tschegg SE, Int J Fatigue, 25, 2003, 245-256

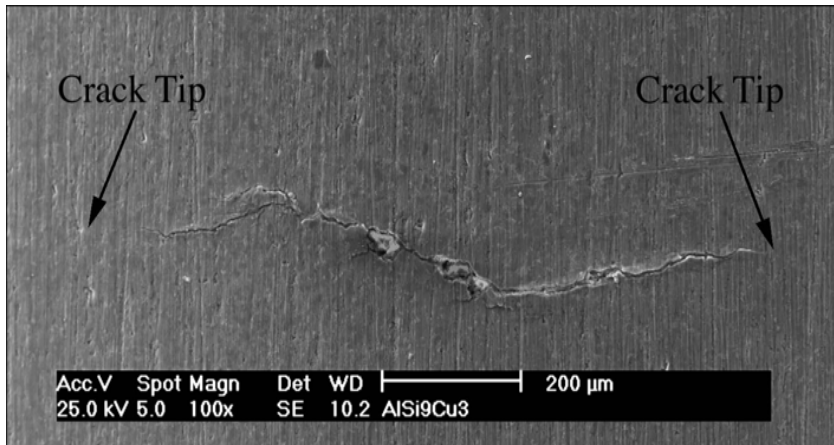


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5 novembre 2008

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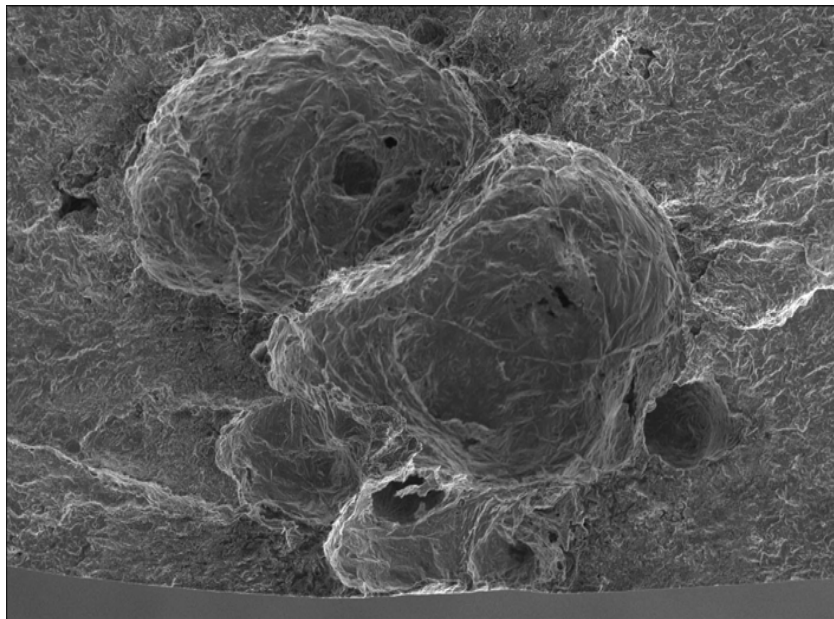


# VHCF Aluminium and Magnesium Alloys



**Non-propagating crack**  
High-pressure die cast **AlSi9Cu3**

1.05x10<sup>9</sup> cycles, 47.5 MPa  
(78 % of mean endurance  
strength at 150 °C)



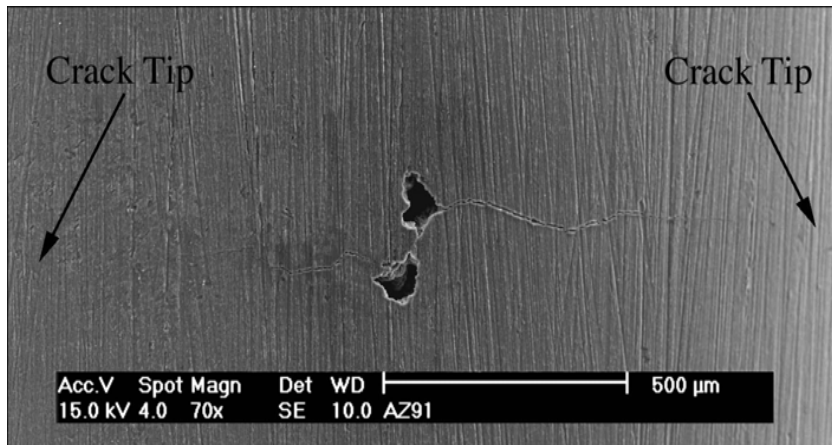
Maximum length of  
non-propagating cracks: 1.2 mm

Fracture surface  
(after increase of load)

Mayer H, Kolloquium Werkstoffe, Fertigung, Konstruktion, Siegen 2004



# VHCF Aluminium and Magnesium Alloys

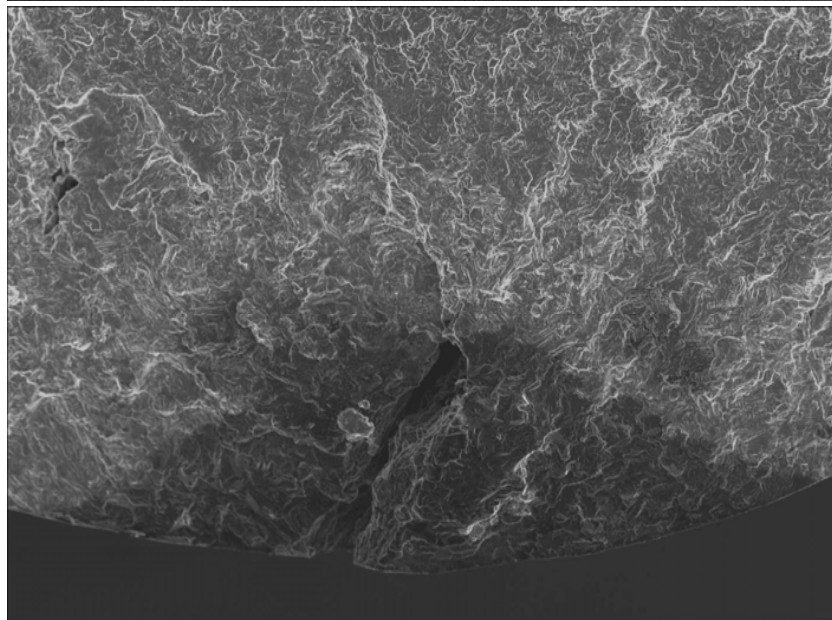


**Non-propagating crack**  
**High-pressure die cast AZ91**

1.51x10<sup>9</sup> cycles, 38 MPa  
(90 % of mean endurance  
strength at 150 °C)

Maximum length of  
non-propagating crack: 1.6 mm

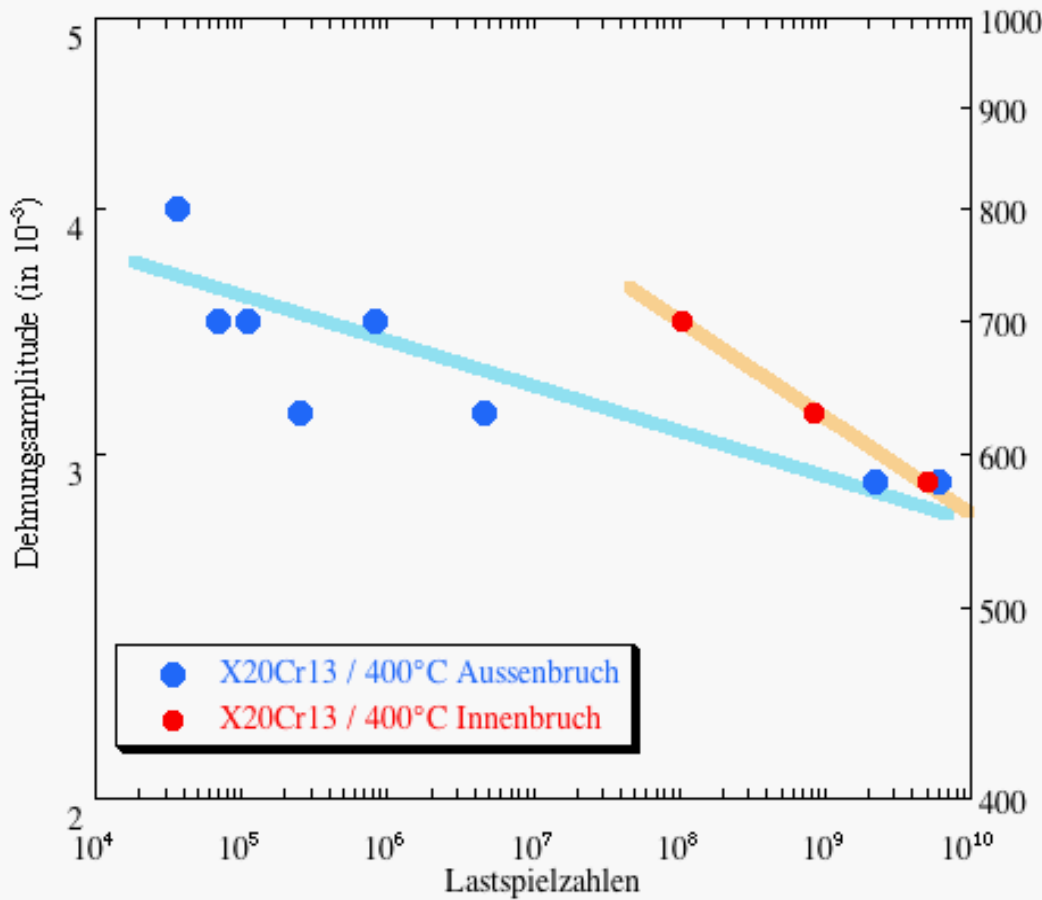
Fracture surface  
(after increase of load)



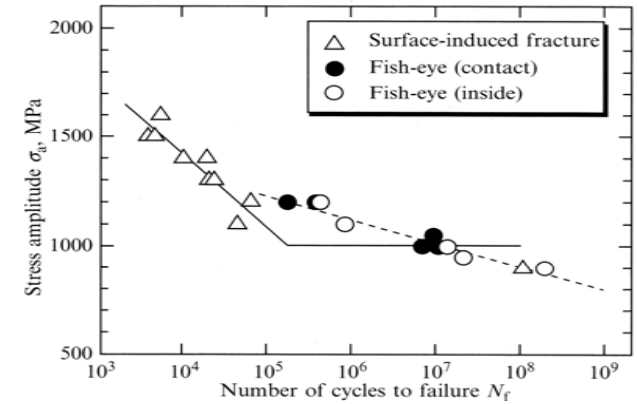
Mayer H, Kolloquium Werkstoffe, Fertigung, Konstruktion, Siegen 2004

# VHCF X20Cr13 Steel

Axial 20 kHz tension-compression loading  
 X20Cr13: 11.3 Cr, 0.2 C, 0.22 Al  
 (940°C /oil quench/ hardening 400°C/2.5 h)



Similar Sakai et al, 2002



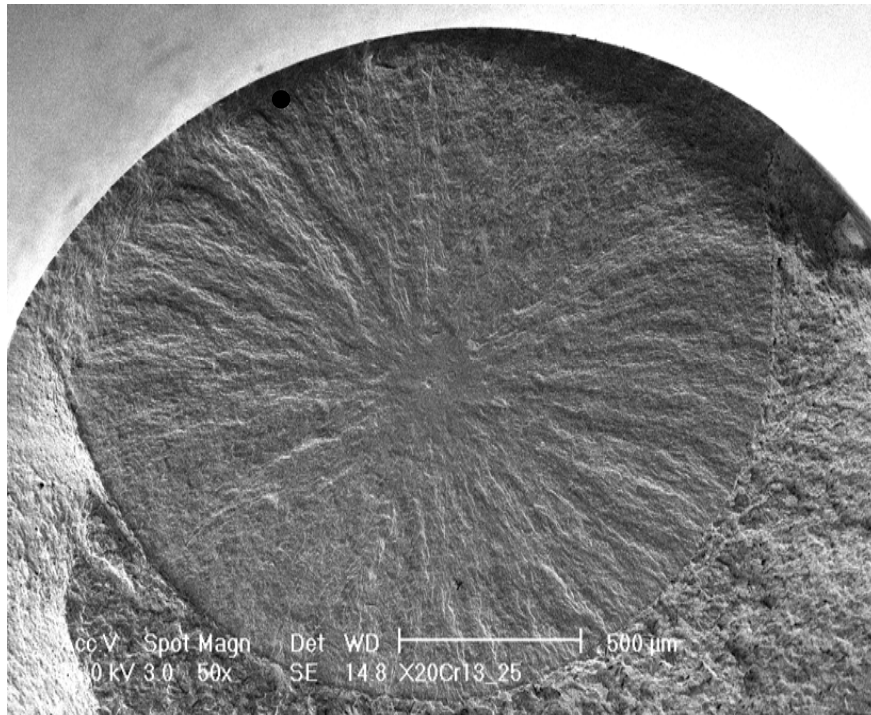
- Crack initiation from surface
- Crack initiation  $\geq 10^8$  cycles from internal inclusions

Stanzl-Tschegg, DGM Meeting Berlin, June 2006

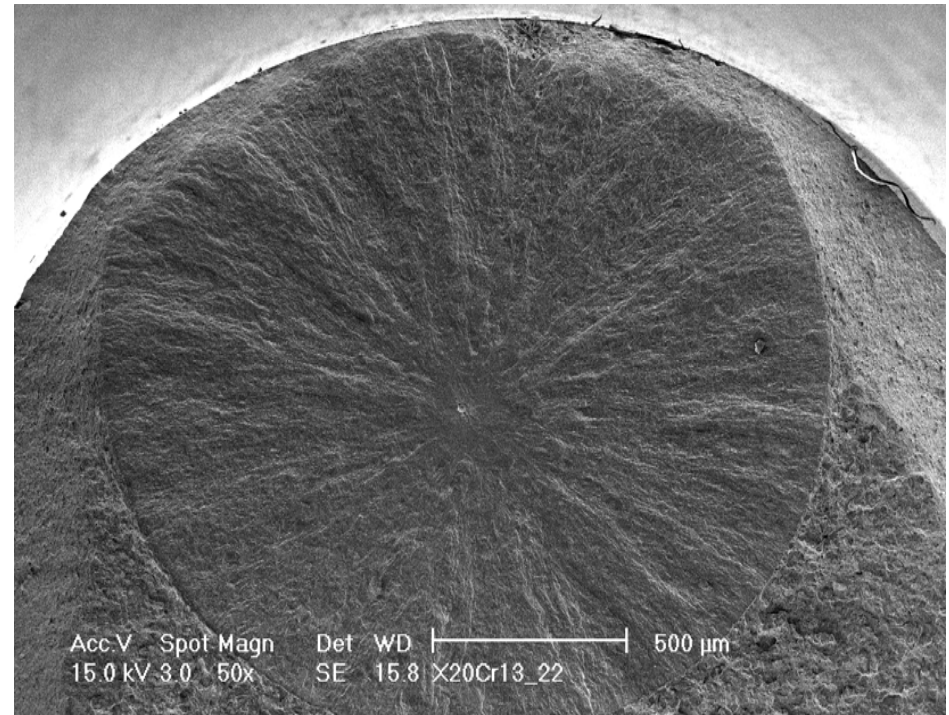
# Crack Initiation from Internal Inclusions

Axial 20 kHz Tension-Compression Loading

X20Cr13: 11.3 Cr, 0.2 C, 0.22 Al (940°C / oil quenched, hardening 400°C/2.5 h)



$\Delta\sigma = 620 \text{ MPa}$ ,  $N_f = 8.48 \times 10^8$



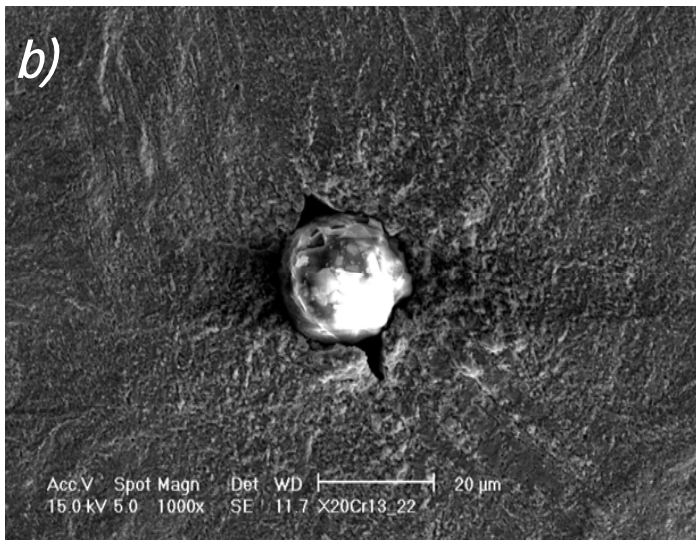
$\Delta\sigma = 700 \text{ MPa}$ ,  $N_f = 1.3 \times 10^8$

Stanzl-Tschegg, DGM Meeting Berlin, June 2006

# Crack Initiation from Interior Inclusions



Crack initiation from ca. 10-20 µm  
 $\text{Al}_2\text{O}_3$ , CaO, MnS, MgO inclusions  
after ca.  $10^8 - 10^9$  cycles



EDAX Analysis (Wt%)

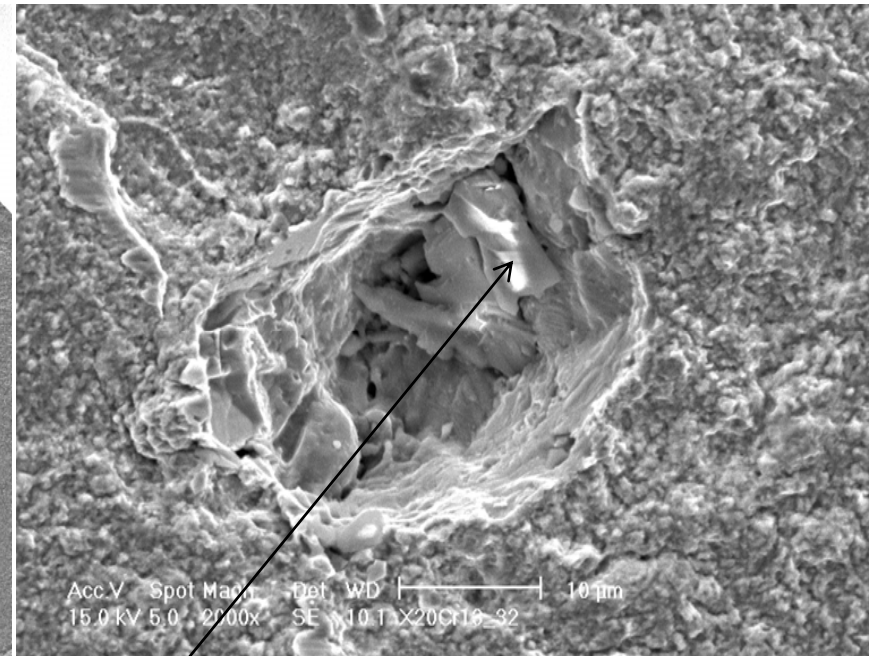
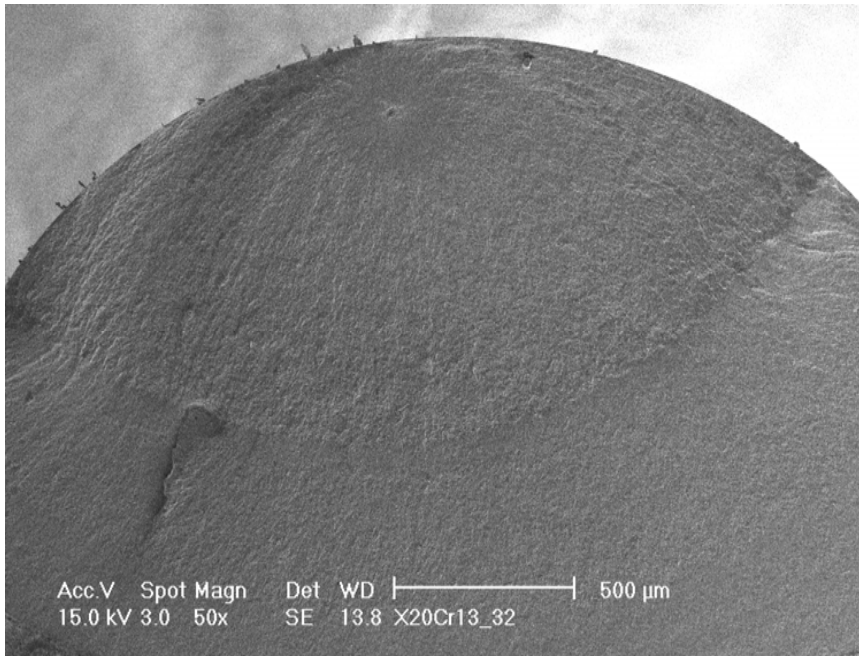
	a)	b)
Al:	22.40	18.44
S:	24.55	27.06
Ca:	17.74	22.59
Mn:	6.96	5.80
Mg	6.07	4.49
Fe:	5.34	8.81

Stanzl-Tschegg, DGM Meeting Berlin, June 2006

# Crack Initiation from Interior Inclusions

Axial 20 kHz Tension-Compression Loading

X20Cr13: 11.3 Cr, 0.2 C, 0.22 Al (940°C / oil quenched, hardening 400°C/2.5 h)

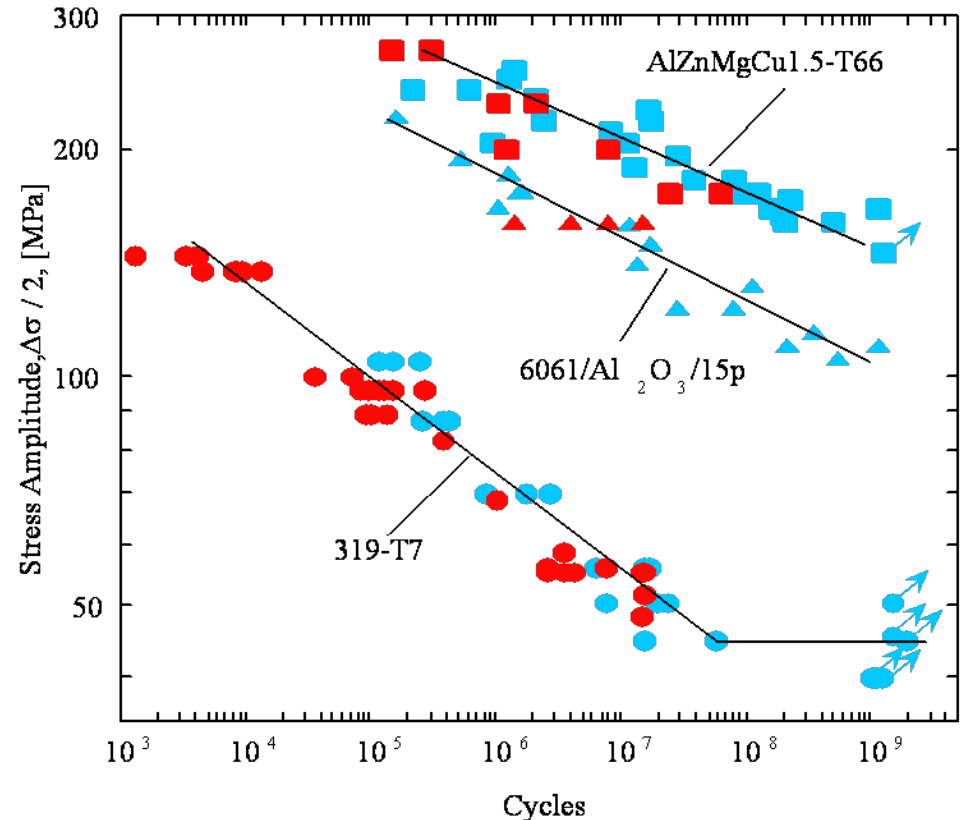
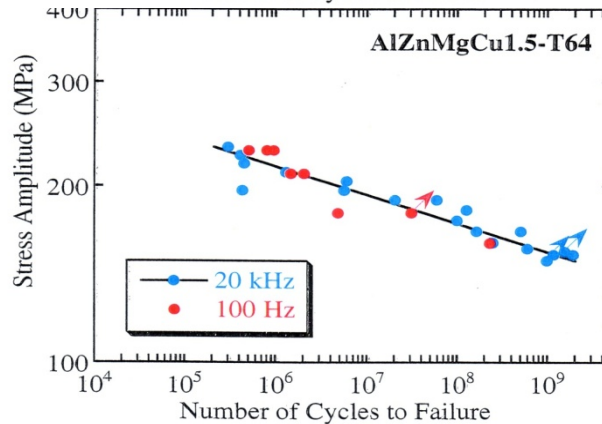
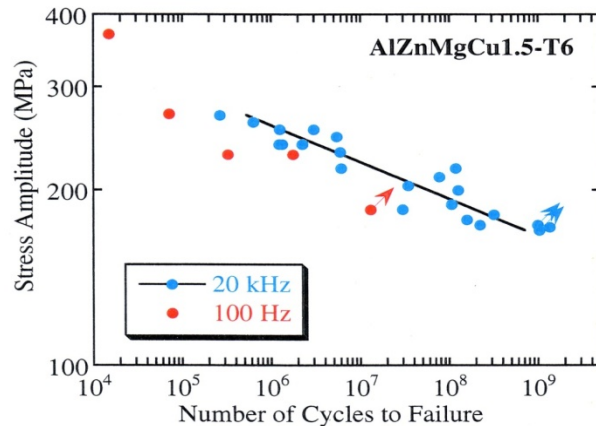


Interior crack initiation from  
Carbide inclusion

EDAX Analysis (wt%) Fe: 64.10  
Cr: 10.01

Stanzl-Tschegg, DGM Meeting Berlin, June 2006

# Frequency Effect? S-N Curves Al alloys



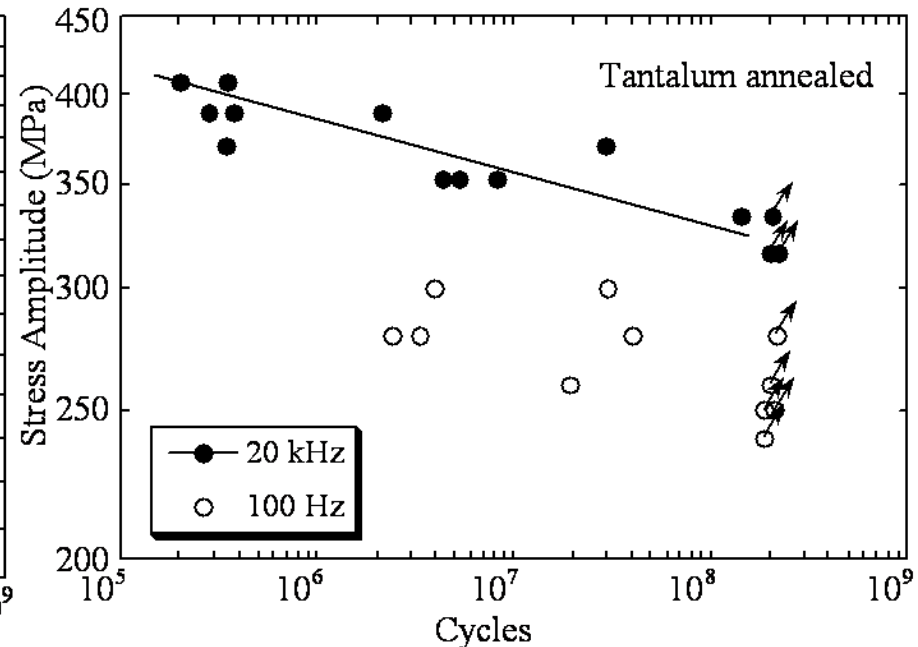
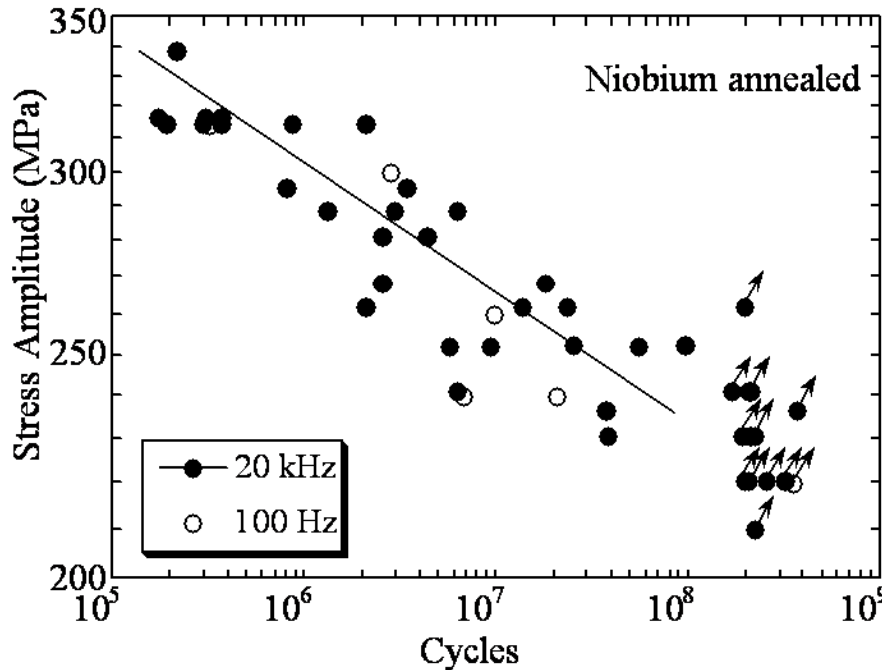
Mayer H, Papakyriacou M, Pippan R,  
Stanzl-Tschegg SE  
Mat Sci Eng A314, 2001, 48-54

**No frequency effect**

Papakyriacou M, Mayer H, Fuchs  
U, Stanzl-Tschegg, Wei RP,  
FFEMS 25, 2002, 887-896

# Frequency Effect?

## S-N Curves Nb and Ta



Papakyriacou M, Mayer H, Plenk H, Pypen C, Stanzl-Tschegg SE, Mat Sci Eng A 308, 2001, 143-152

Yield strength  $R_{p0.2} = 385$  MPa

Endurance limit at  $2 \times 10^8$  cycles:

240 MPa - 20 kHz    220 MPa - 100 Hz

**Niobium: No frequency effect**

Yield strength  $R_{p0.2} = 240$  MPa

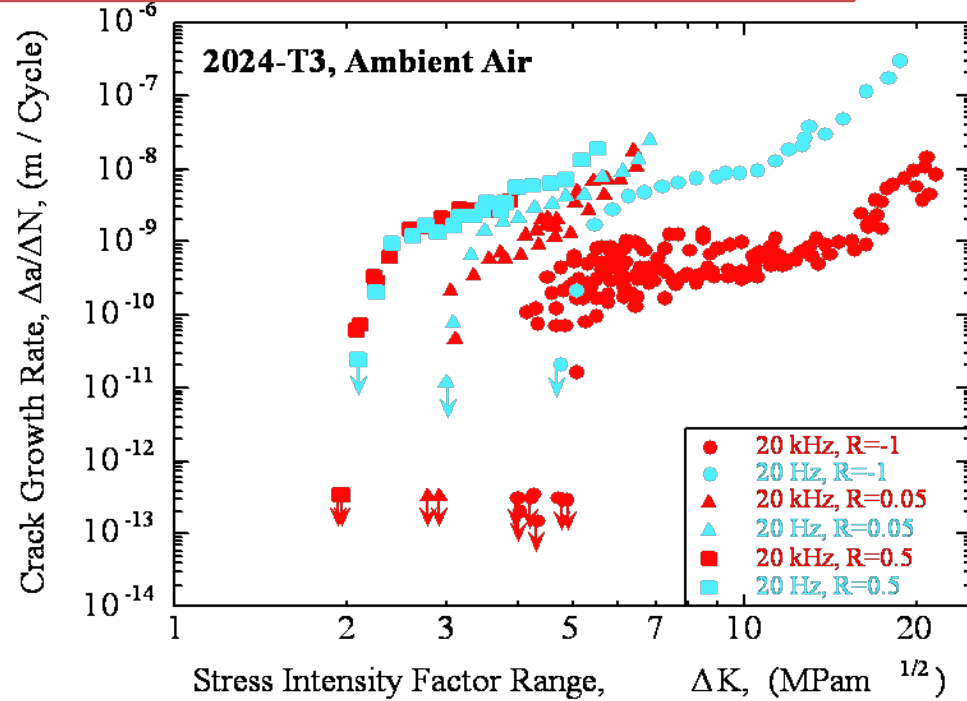
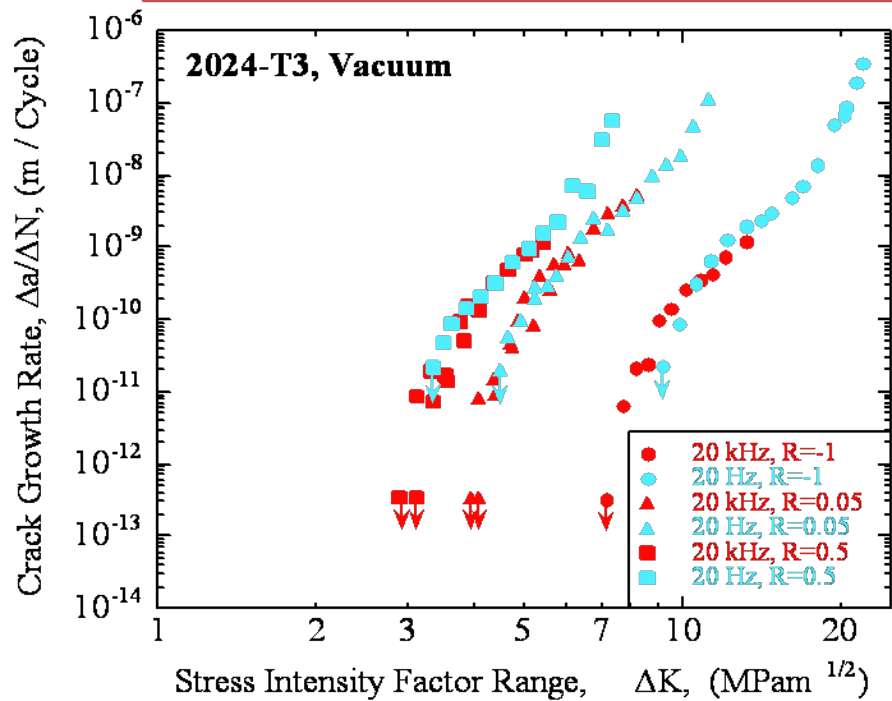
Endurance limit at  $2 \times 10^8$  cycles:

365 MPa - 20 kHz    290 MPa - 100 Hz

**Tantalum: Frequency effect**

# Frequency Effect?

## Fatigue Crack Growth in Humid Air



Holper B, Mayer H, Vasudevan AK, Stanzl-Tschegg, Int J Fatigue, 26, 2004, 27-38

- **No** influence of plastic deformation rate on  $\Delta a/\Delta N$  (**vacuum**)
- **Frequency effect** at  $\Delta a/\Delta N > \text{ca. } 10^{-9}$  m/cycle owing to air **humidity**
- **No frequency effect** on  $\Delta K_{\text{threshold}}$



# Frequency Effect on S-N and $\Delta a/\Delta N$ curves - Summary

## Frequency effect present

- At high loads close to yield stress (e.g. Tantalum!)  
→ Testing of strongly damping material problematic
- At higher crack growth rates in corrosive environment

## No frequency effect

- Al-alloys
- High-strength steels
- Titanium alloys Ti-6Al-7Nb and Ti-6Al-4V
- Mg – high pressure die cast alloy

# Mechanisms of Fatigue Damage

**Crack initiation** mostly from **SURFACE IMPERFECTIONS** like



notches,  
scratches



inclusions



PSBs



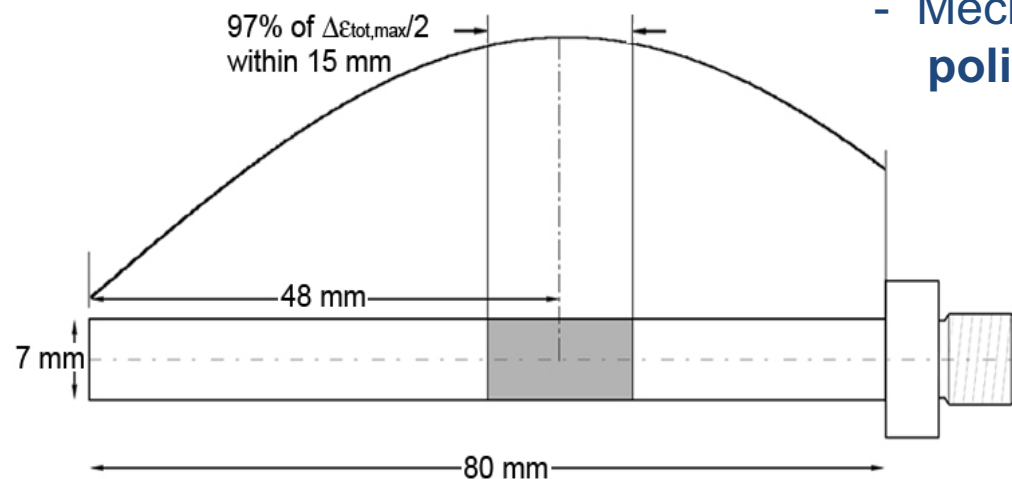
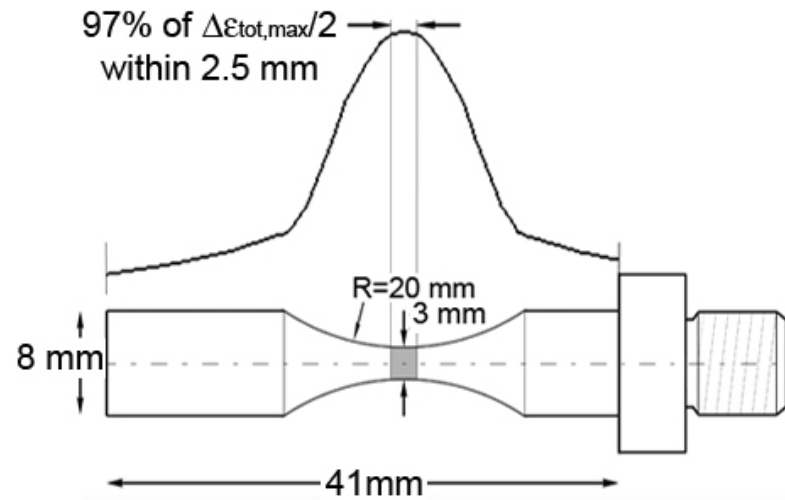
or from **INSIDE**



inclusions,...

**Relevance of PSBs in copper for crack initiation, propagation and life times (endurance limit?) in the VHCF range**

# Material and Specimen Shape



- **Electrolytic copper** (DIN1787/17672/1756)
- Cylindrical, 7 mm diameter, 80 mm long Hourglass **shape**, inner diameter: 3mm
- 750°C /75 min, vacuum/ air cooled
- **Mean grain size**: approximately 60  $\mu\text{m}$
- Mechanical and electrolytical **polishing** (2V, 42 mA/cm<sup>2</sup>)
- **Calibration:**  
Induction sensor at specimen end  
Strain gages along the whole specimen length to measure total axial strain amplitudes  $\varepsilon_{tot}$

# Experimental Procedure

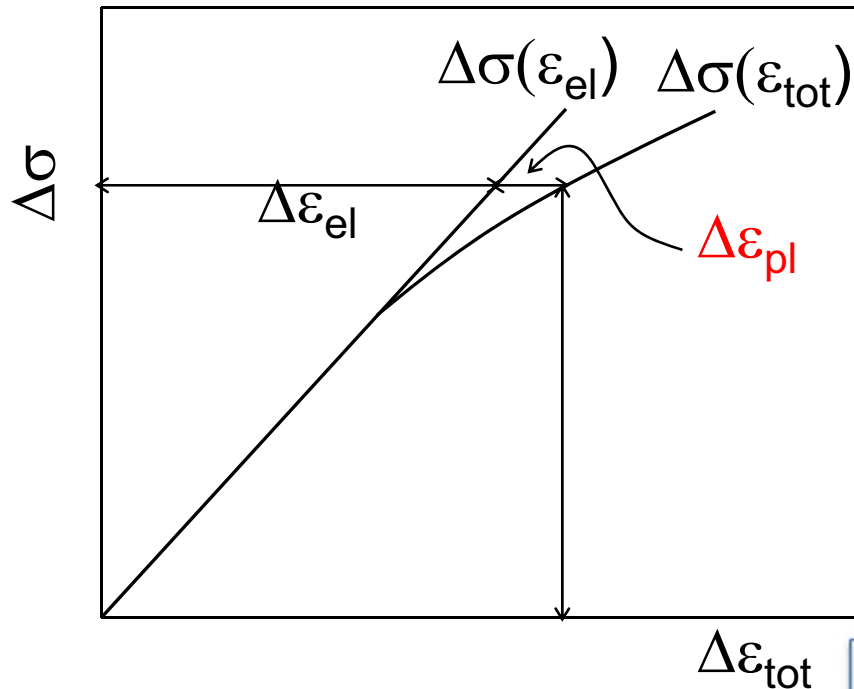
## Ultrasonic test:

- Not stress ( $\Delta\sigma/2$ ) controlled, but
- Displacement or **total strain ( $\Delta\varepsilon_{tot}/2$ )** (strain rate,  $\Delta\varepsilon'_{tot}/2$ ) **controlled**
- **Plastic strain ( $\Delta\varepsilon_{pl}/2$ )** control not possible

*Therefore* →

1. step: Calibration: Determine  $\Delta\varepsilon_{pl}/2$
2. step: Experiment: Ramp loading

# Determination of Stress Amplitude $\Delta\sigma/2$ in “ductile” material



Hooke's Law:

$$E = \Delta\sigma / \Delta\varepsilon_{el}$$

and with:

$$\Delta\varepsilon_{tot} = \Delta\varepsilon_{el} + \Delta\varepsilon_{pl}$$

$\Delta\varepsilon_{el}/2$       elastic cyclic strain  
 $\Delta\varepsilon_{pl}/2$       plastic cyclic strain  
 $\Delta\varepsilon_{tot}/2$       total cyclic strain  
 $\Delta\sigma/2 = \Delta\sigma_{el}/2$       cyclic stress  
 $E = 130 \text{ GPa}$  Young's modulus

$$\Delta\varepsilon_{tot}/2 = \Delta\varepsilon_{el}/2 + \Delta\varepsilon_{pl}/2$$

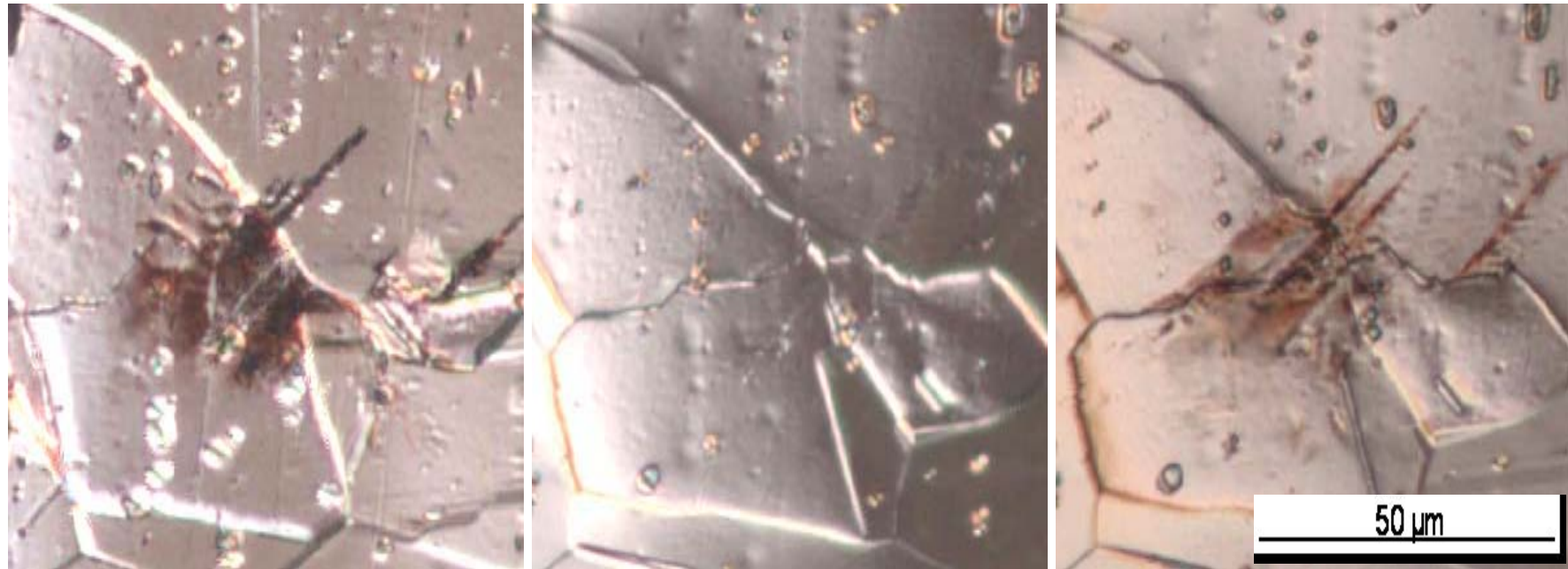
$$\rightarrow \Delta\sigma/2 = E \cdot (\Delta\varepsilon_{tot}/2 - \Delta\varepsilon_{pl}/2)$$

$$= E \cdot \Delta\varepsilon_{el}/2$$

# Identification of PSBs: Re-appearance of Slip Bands after Electropolishing PSBs and Reloading

→ „Conventional“ PSB threshold

$$\Delta\sigma/2 \approx 63 \text{ MPa} \quad (\Delta\varepsilon_{pl}/2 \approx 6.1 \times 10^{-6})$$



**Initial loading  $2 \times 10^6$**

Load direction: top to bottom.

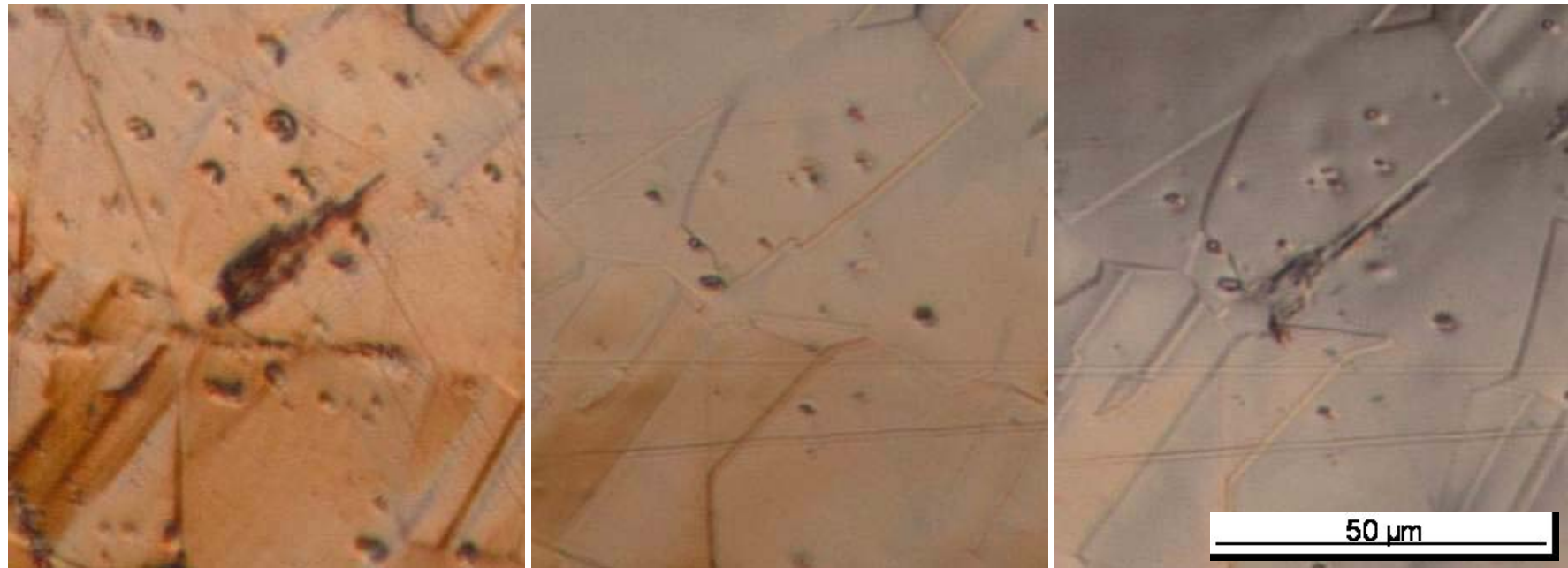
**After polishing**

**+ Reloading  $2 \times 10^6$  cycles**

# PSBs in VHCF range also *below* PSB threshold

→ „VHCF“ PSB threshold

$$\Delta\sigma/2 \approx 45 \text{ MPa } (\Delta\varepsilon_{pl}/2 \approx 3.6 \times 10^{-6}), N \approx 2 \times 10^8$$



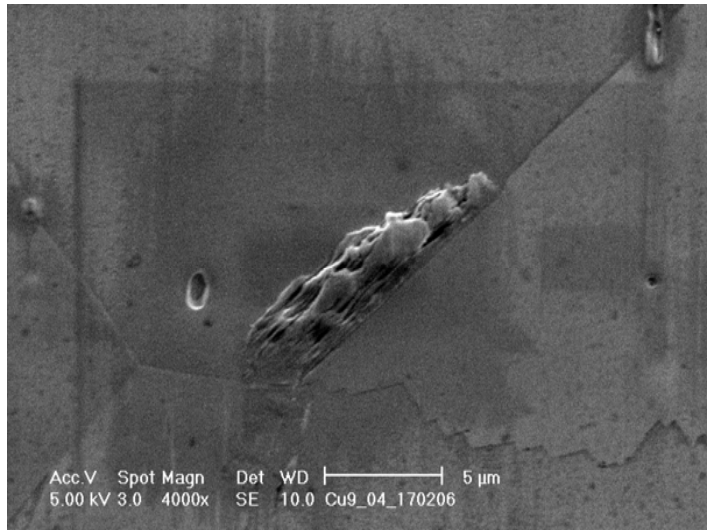
$$\Delta\sigma/2 \approx 50 \text{ MPa } (\Delta\varepsilon_{pl}/2 \approx 4.1 \times 10^{-6})$$

Initial loading  $2 \times 10^8$  cycles  
(Load direction: top to bottom)

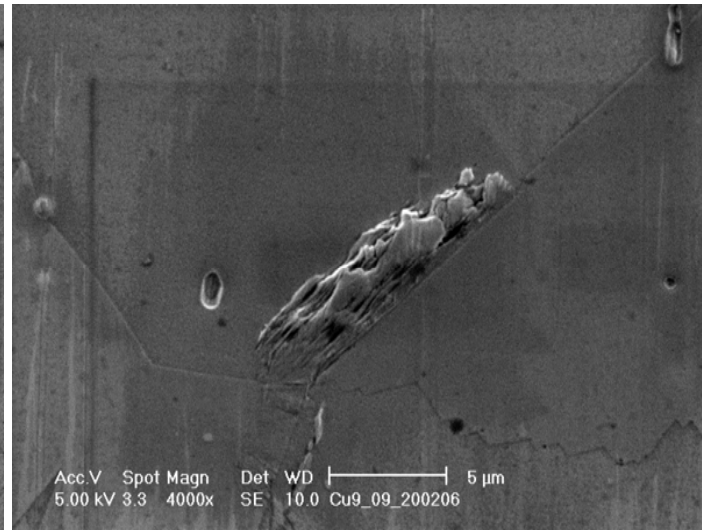
After polishing

+ Reloading  $2 \times 10^6$  cycles

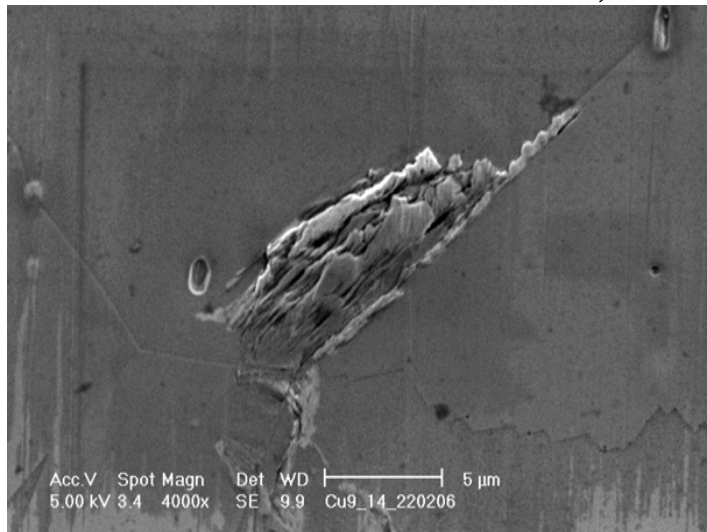
# Structure and Development of PSBs (SEM)



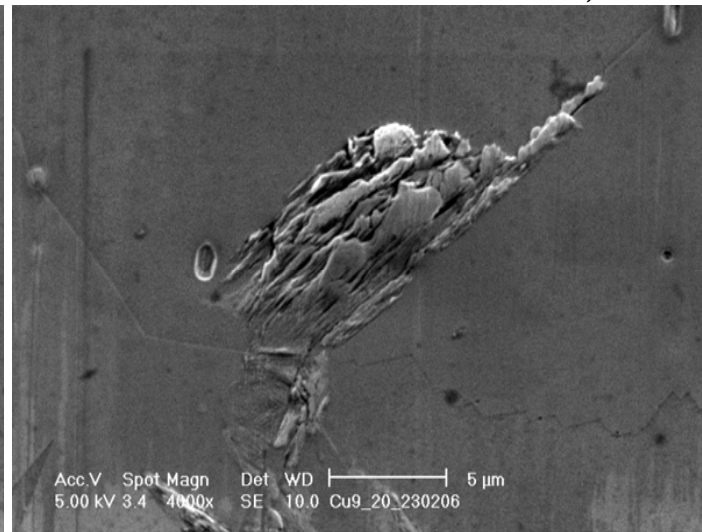
$N = 7,0 \times 10^6$



$N = 1,0 \times 10^7$



$N = 5,0 \times 10^7$



$N = 1,0 \times 10^8$

$\Delta\sigma = 59,2 \text{ MPa}$

~ 3.0 MPa  
below  
PSB  
threshold



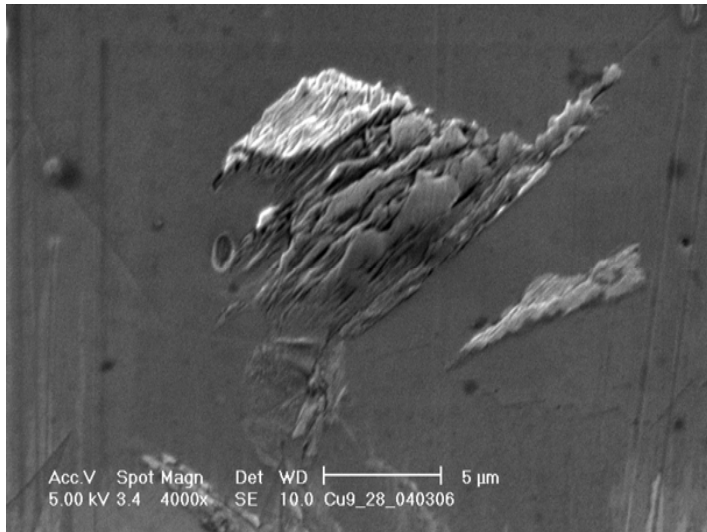
Torino  
5 novembre 2008

Stefanie Stanzl-Tschegg

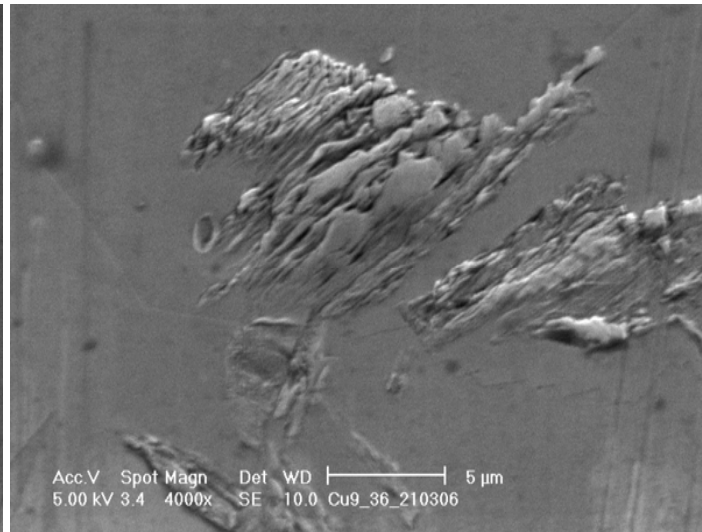




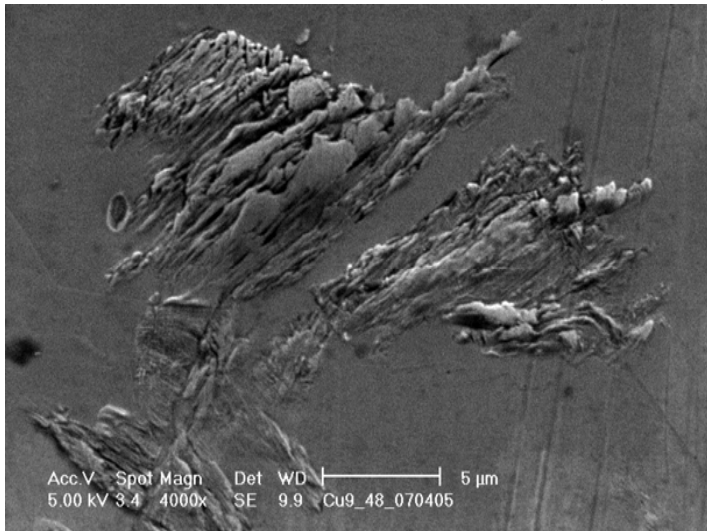
# Structure and Development of PSBs (SEM)



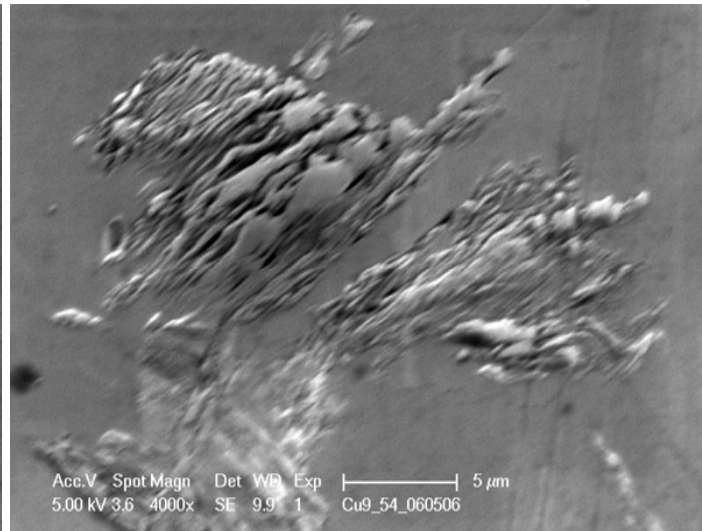
$N = 3,3 \times 10^8$



$N = 5,0 \times 10^8$



$N = 1,0 \times 10^9$

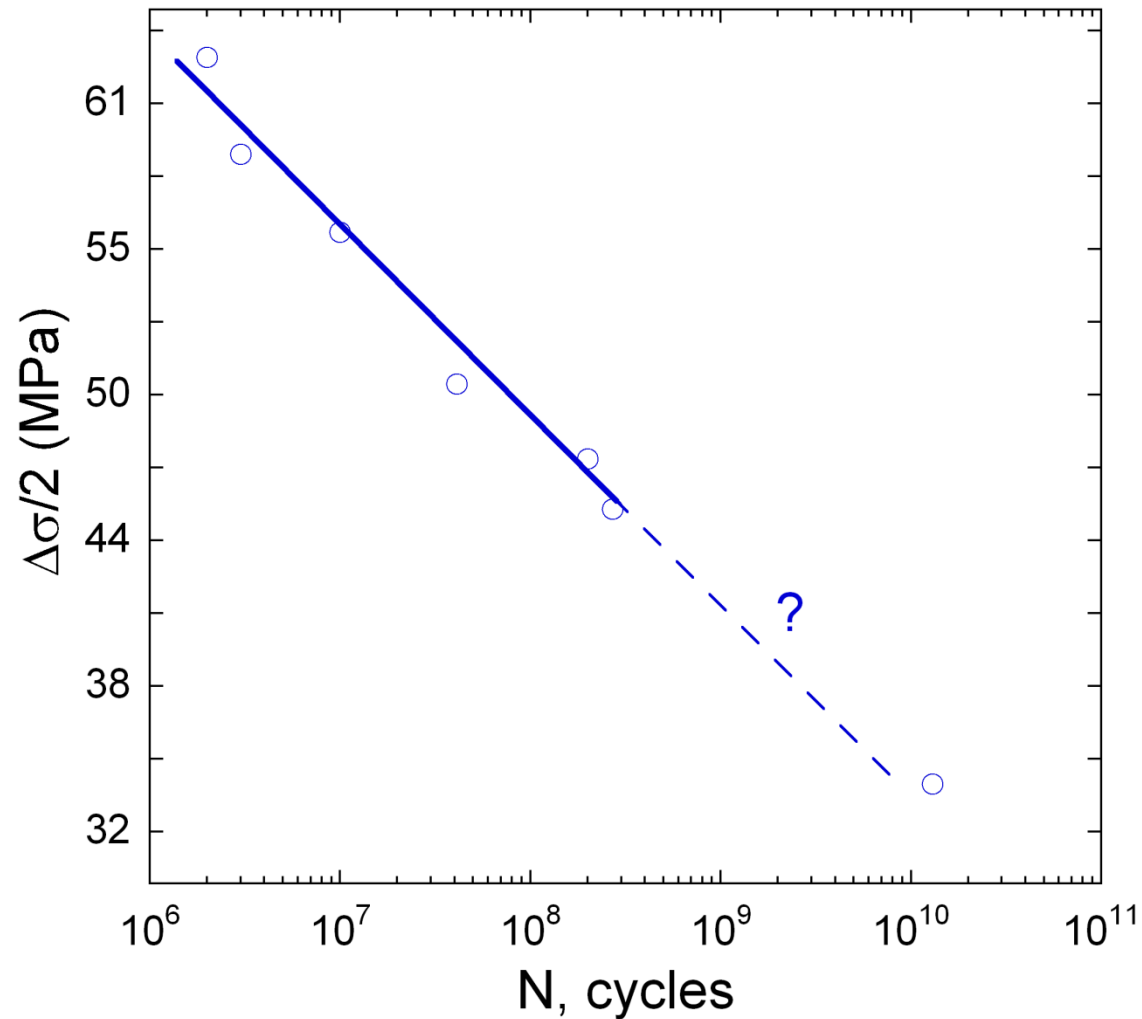


$N = 2,0 \times 10^9$

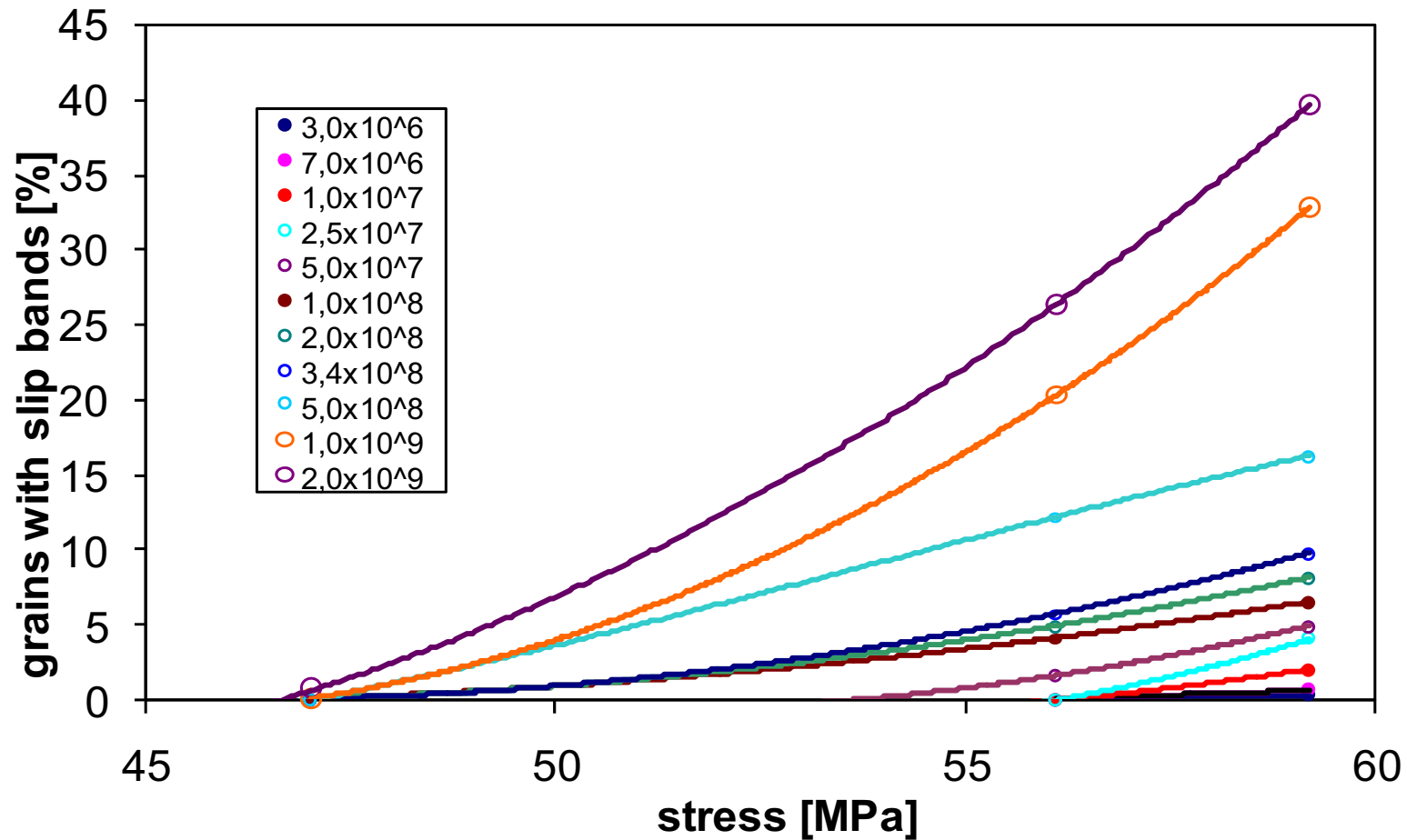
$\Delta\sigma = 59,2 \text{ MPa}$

~ 3.0 MPa  
below  
PSB  
threshold

# Slip Band Formation at and below PSB Threshold: Appearance of first (P)SB

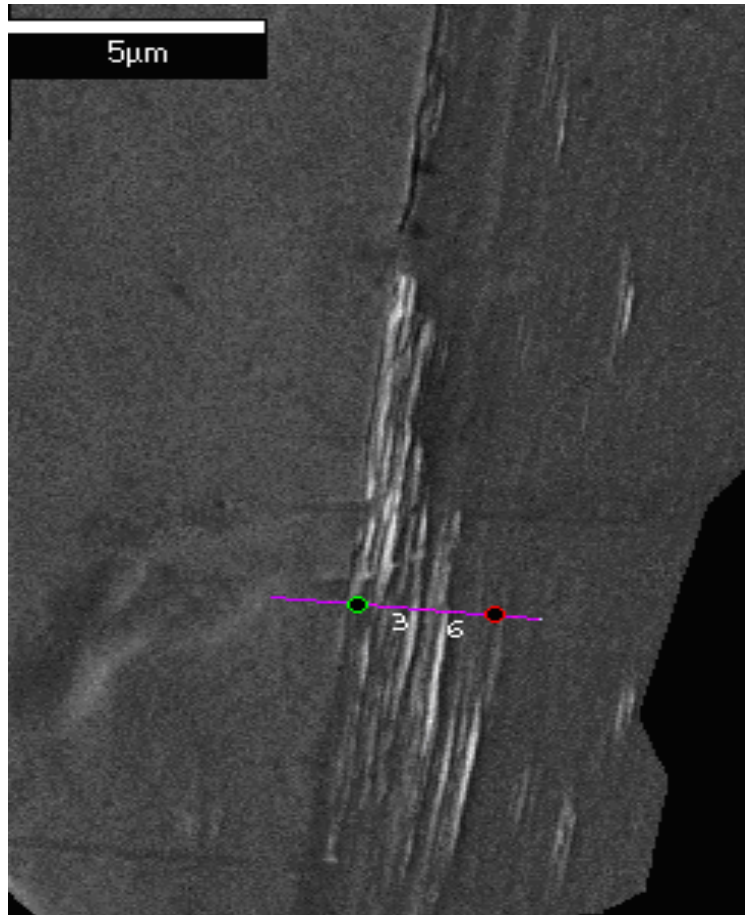


# Increasing Number of PSBs with $\Delta\sigma/2$ and N



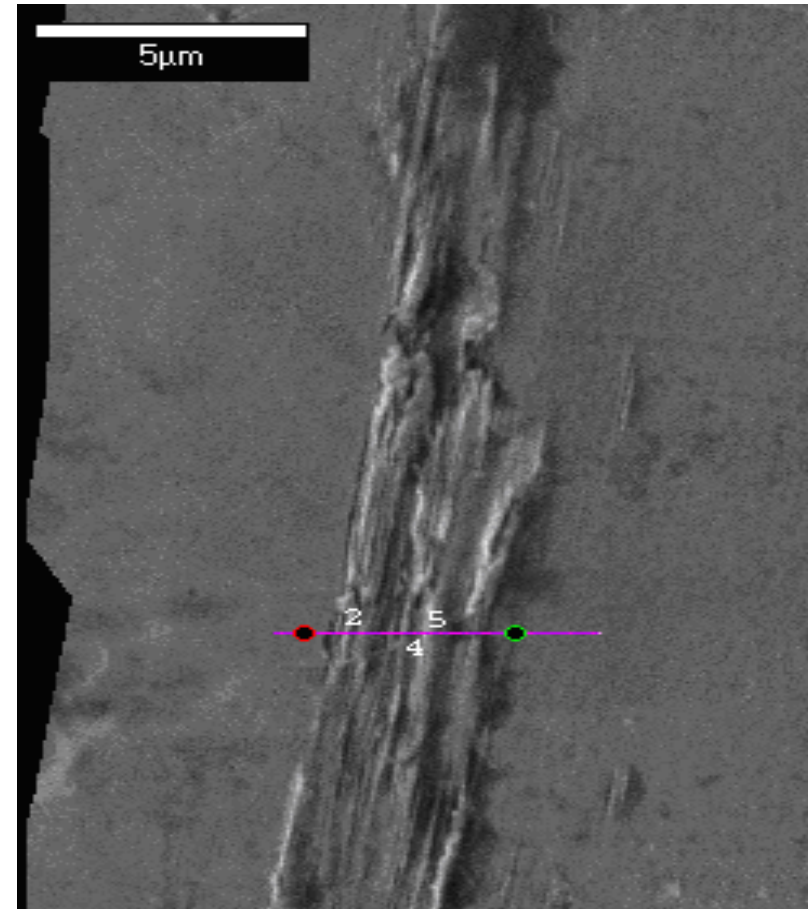
# PSB Structure and Surface Roughness

Measurement: **SEM and MeX – 3D** profile analysis software



$\Delta\sigma/2 = 62.1$  MPa

$N = 5 \times 10^7$  cycles



$\Delta\sigma/2 = 62.1$  MPa

$N = 5 \times 10^8$  cycles

# PSB Structure and Surface Roughness

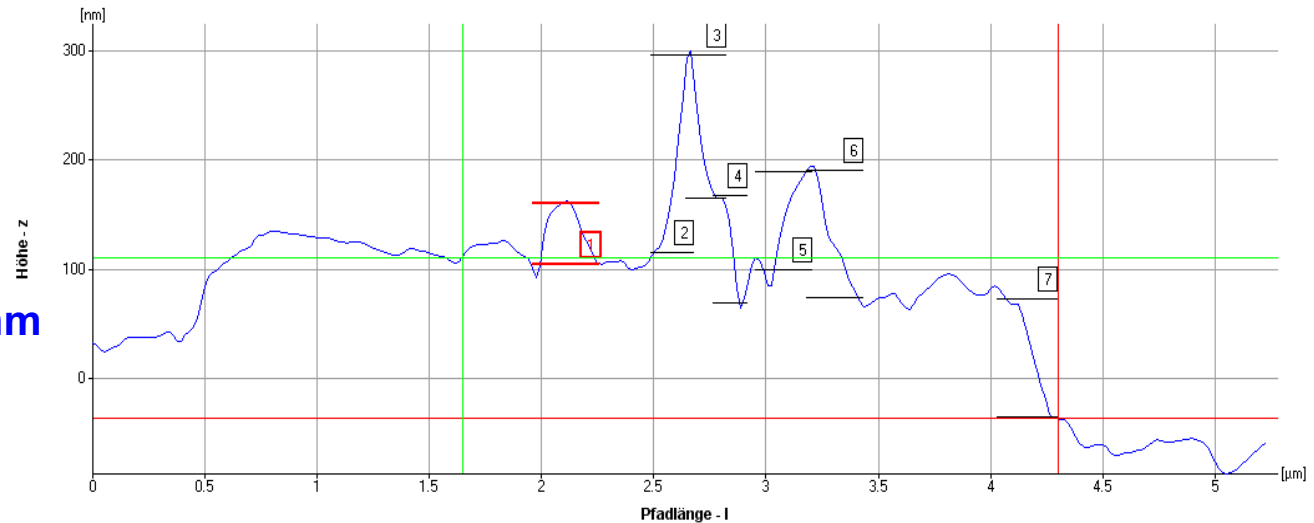
Measurement: **SEM and MeX – 3D** profile analysis software

$\Delta\sigma/2 = 62.1$  MPa

$N = 5 \times 10^7$  cycles

mean height = **111,83 nm**

RMS = 117,49 nm

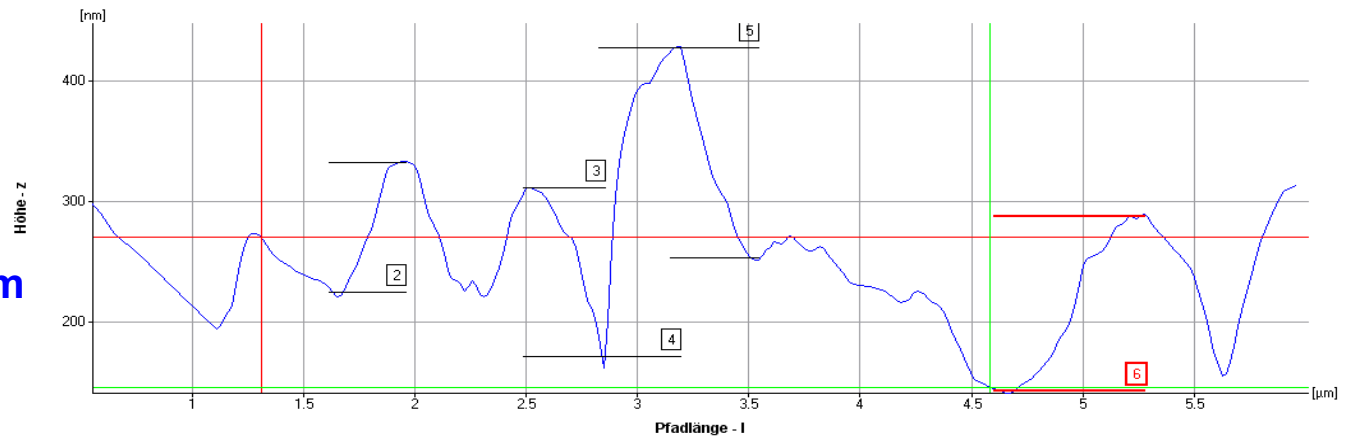


$\Delta\sigma/2 = 62.1$  MPa

$N = 5 \times 10^8$  cycles

mean height = **164,8 nm**

RMS = 172,38 nm



Torino  
5 novembre 2008

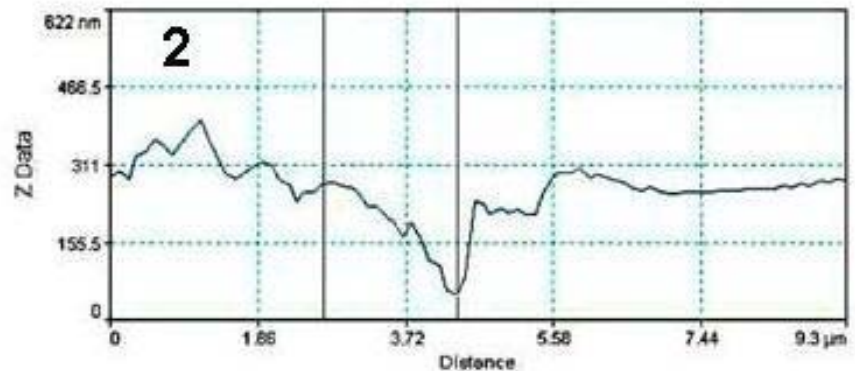
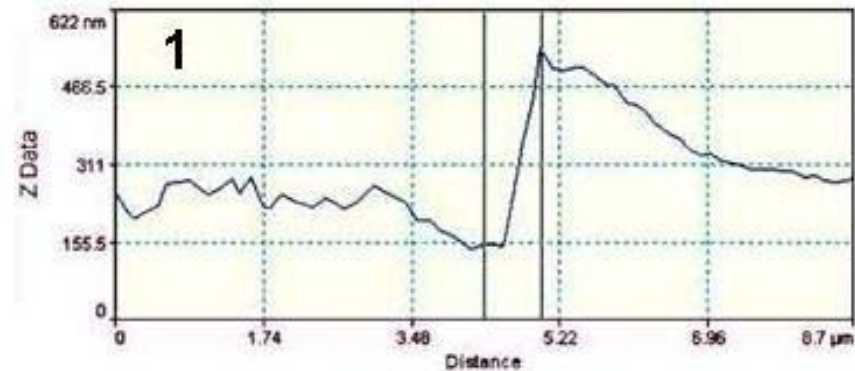
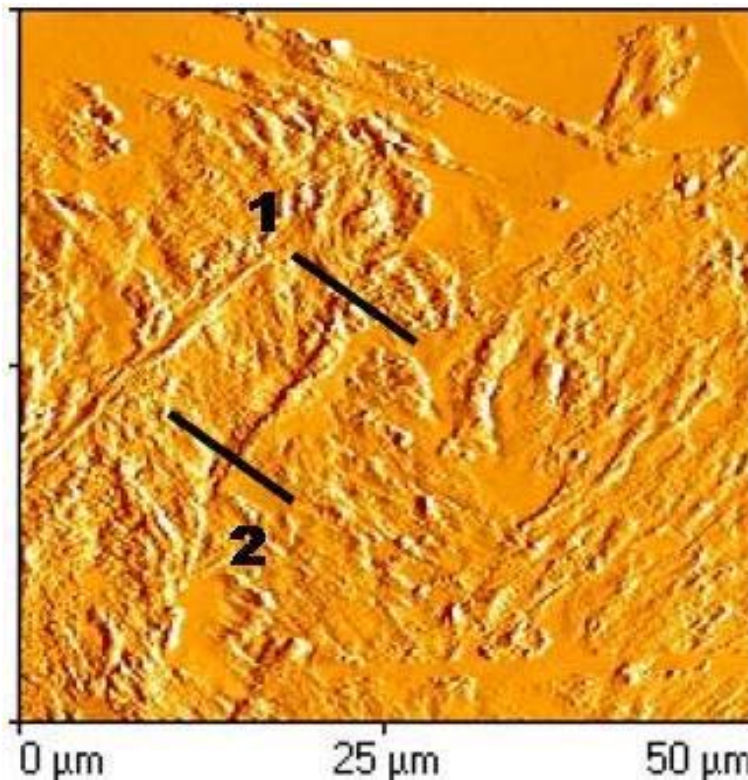
Stefanie Stanzl-Tschegg



# Measurement of Surface Roughness

## AFM Topometric Explorer

in contact mode, set point 10 nA, Si<sub>3</sub>N<sub>4</sub> pyramid tip, 50° angle, 50 nm radius

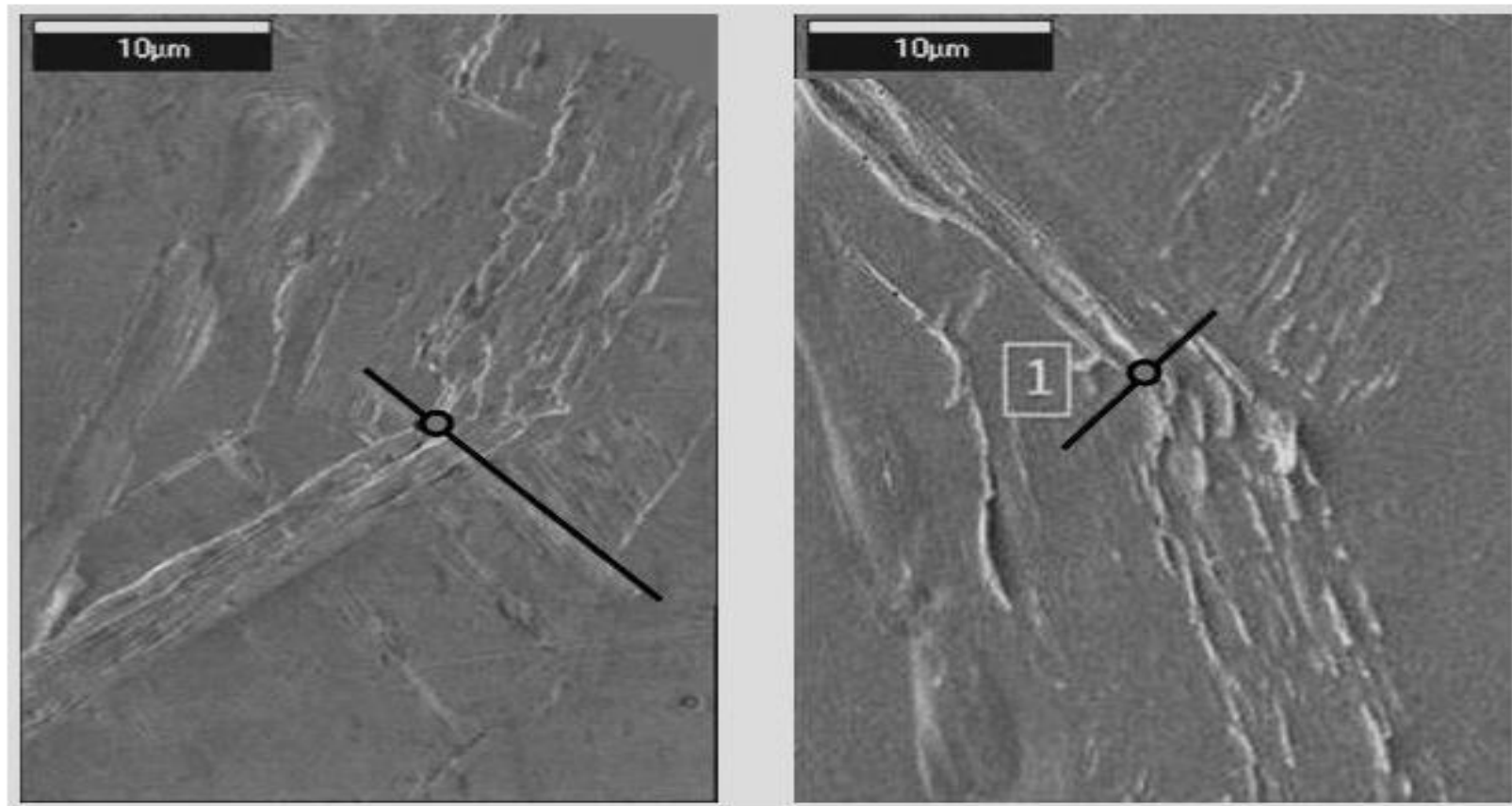


$\Delta\sigma/2 = 53 \text{ MPa}$ ,  $N = 1,28 \times 10^9$  cycles

$h_{\max} \sim 400 \text{ nm}$ ,  $h_{\min} \sim 230 \text{ nm}$

# PSB Structure and Surface Roughness

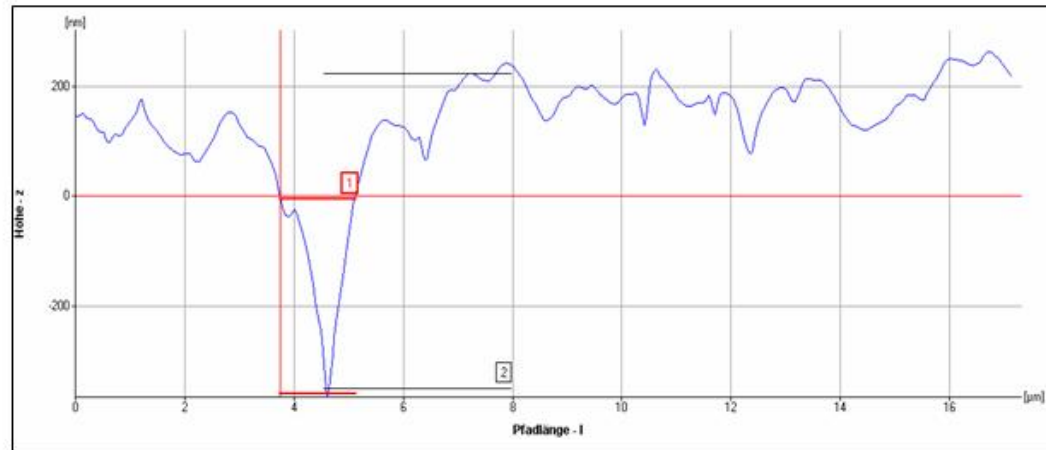
## Plastic replica and SEM



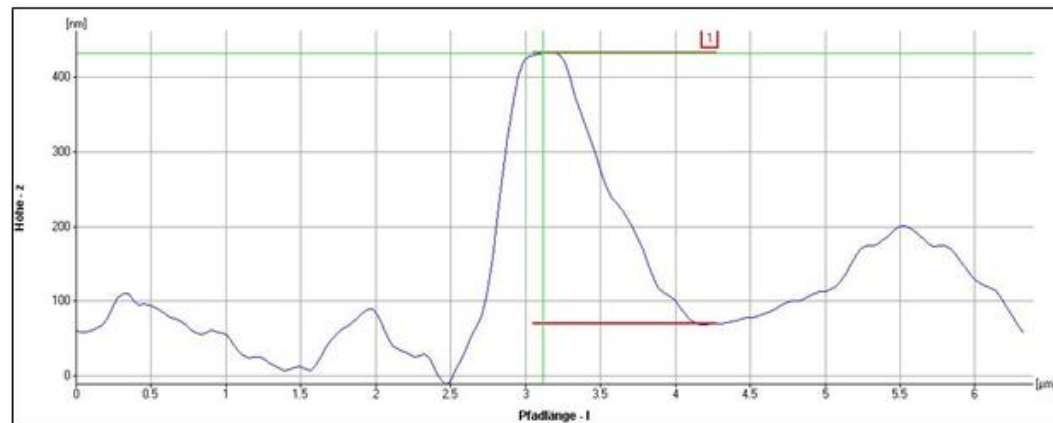
$\Delta\sigma/2 = 100 \text{ MPa}$ ,  $N = 1 \times 10^7$  cycles

# Surface Roughness

MeX – 3D profile analysis software



(a)



(b)

$$\Delta\sigma/2 = 100 \text{ MPa}$$

$$N = 1 \times 10^7$$

Direct SEM:

Intrusion depth:

353 nm

Replica:

Intrusion depth:

362 nm



# Summary: Surface Roughness

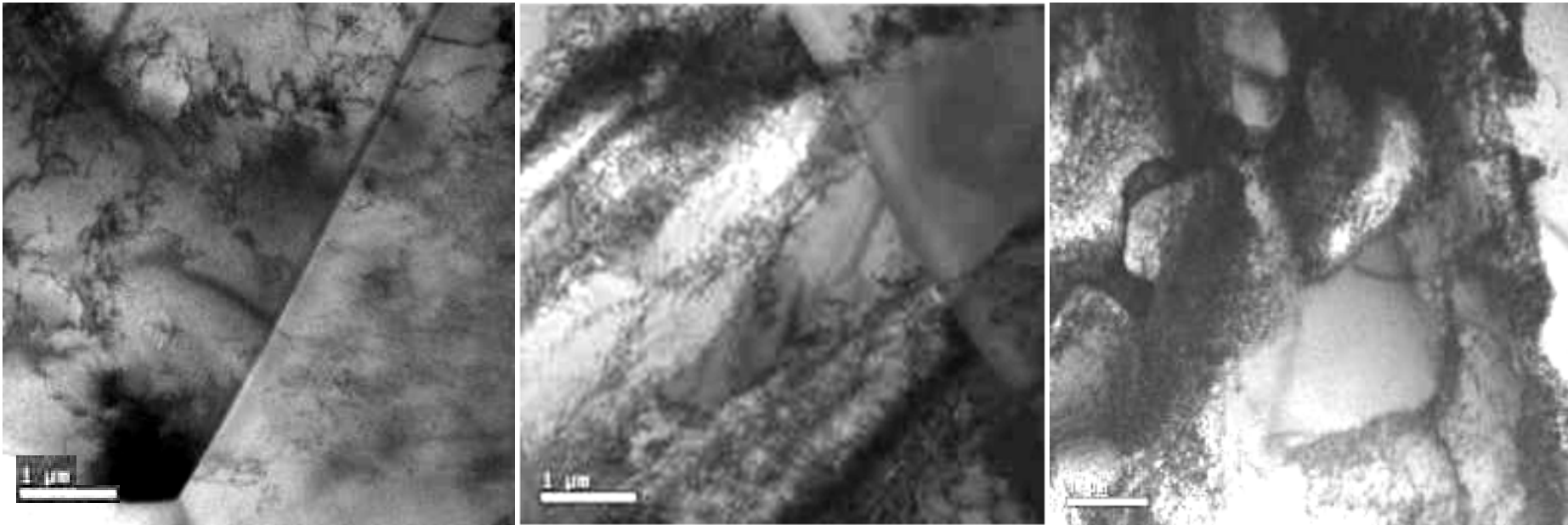
Increase of surface roughness with  $\Delta\sigma/2$  and N

$\Delta\sigma/2$	Roughness		
	Mean	Min.	Max.
34 MPa	~ 20 nm	~ 14 nm	~ 30 nm
↓	↓	↓	↓
60 MPa	~ 200 nm	~ 80 nm	~ 350 nm
↓	↓	↓	↓
100 MPa	~ 400 nm	~200 nm	~1000nm

E.g. **Surface roughness ~ 200 nm** for  $\Delta\sigma/2 \sim 60\text{MPa}$ ,  $N \sim 10^{10}$  (mean of three measuring techniques) - **high local variation**.

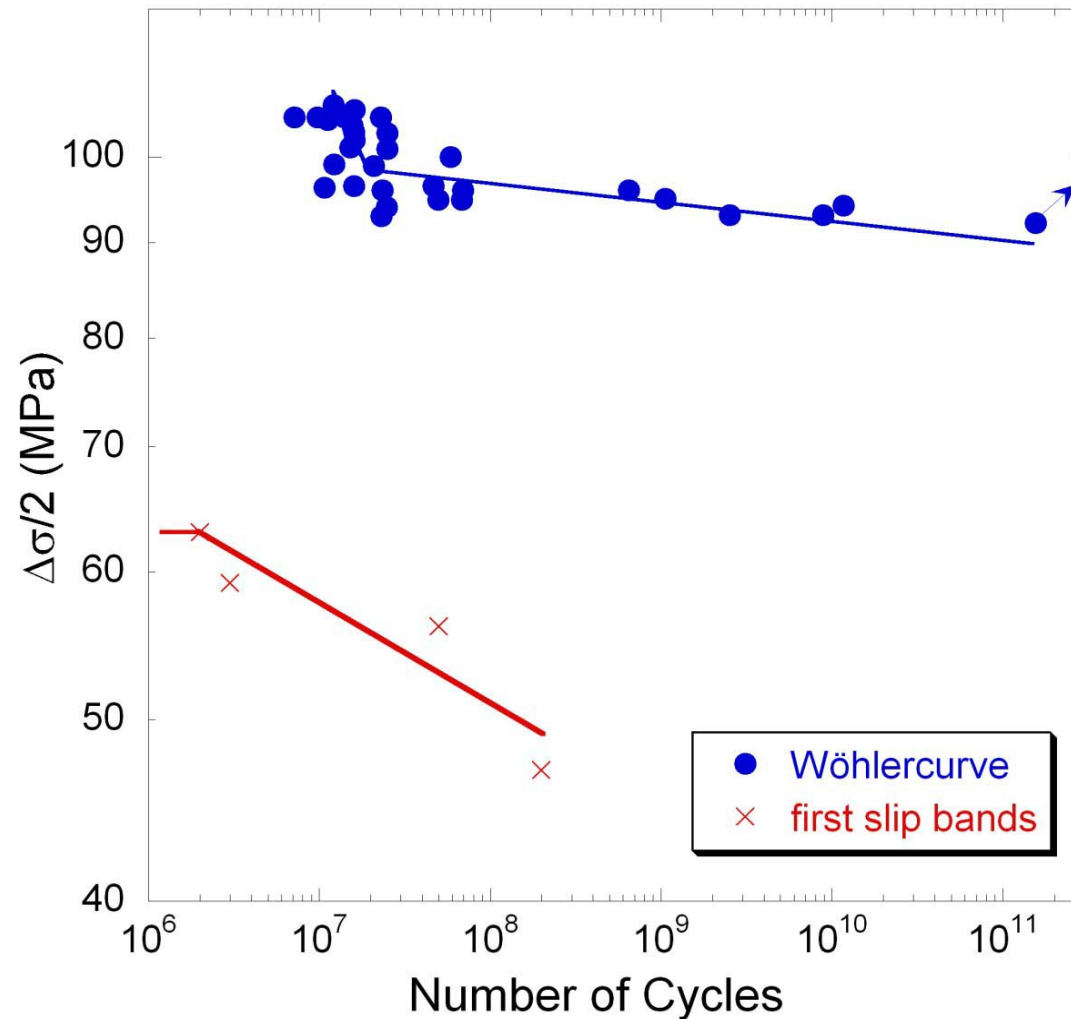
# Dislocation structure (TEM)

$\Delta\sigma/2 \approx 64 \text{ MPa}$  ( $\sim 1 \text{ MPa}$  above PSB Threshold ( $\leq 63 \text{ MPa}$ ))  
 $1,5 \times 10^{10}$  cycles



Dislocations clusters and cells

# Fatigue life diagram, 19 kHz: Wöhler (S-N) plot



## Failure:

$\Delta\sigma/2 \sim 93-97$  MPa

$N_f \sim 3 \times 10^7 - 1.1 \times 10^{10}$

## No failure:

$\Delta\sigma/2 \leq 92.2$  MPa

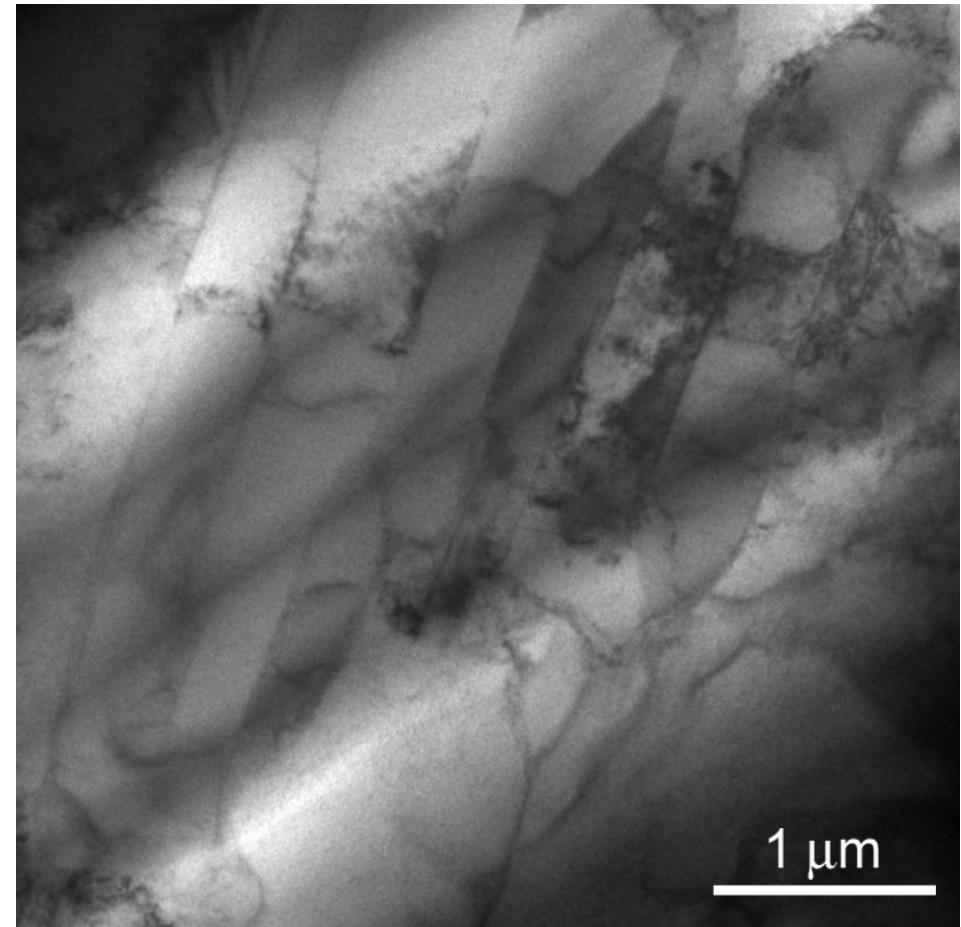
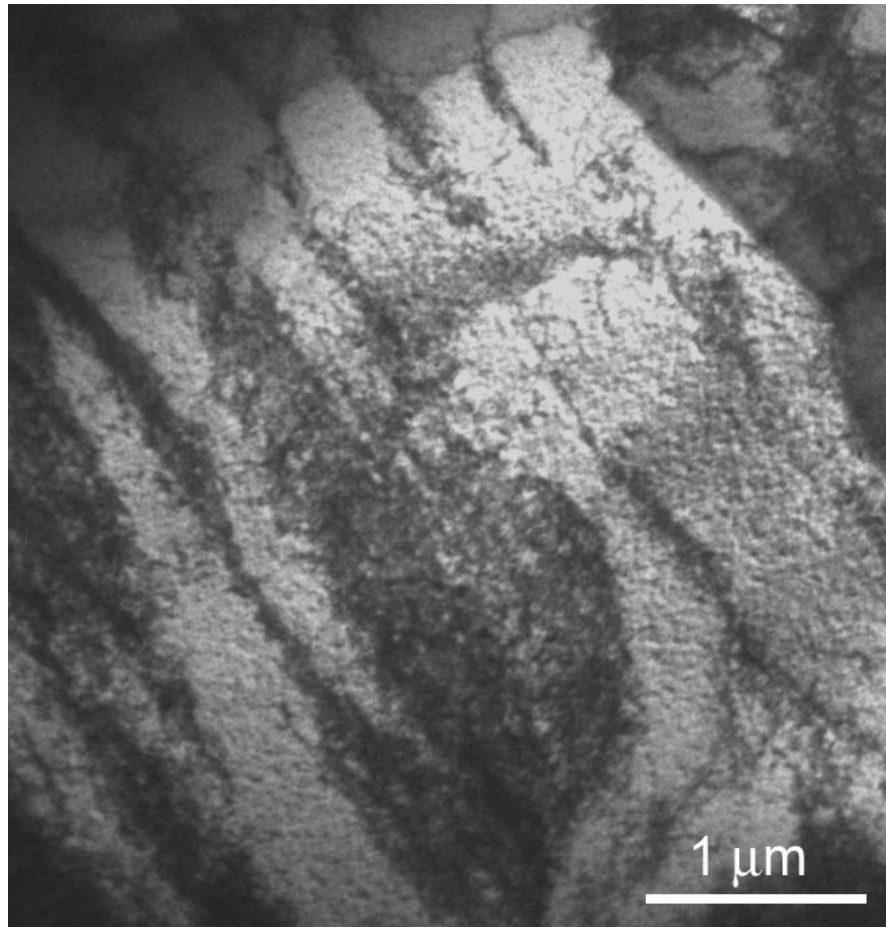
until  $N = 1.7 \times 10^{11}$  cycles

## „VHCF“ PSBs:

$\Delta\sigma/2: \sim 45 - 61.7$  MPa

$N \sim 10^6 - 2 \times 10^8$  cycles

# Dislocation structure (TEM) close to endurance limit



$\Delta\sigma/2 \approx 94 \text{ MPa}$ ,  $N = 1,2 \times 10^{10}$  ~ 1 MPa above fatigue limit ( $\leq 93 \text{ MPa}$ )

# PSB Threshold (“conventional” as well as “VHCF”) and Endurance Limit are Different

	„Conventional“ PSB Threshold ( $N \sim 10^6$ )	„VHCF“ PSB Threshold ( $N \sim 2.6 \times 10^8$ )	„Endurance Limit“ ( $N_f = 1.14 \times 10^{10}$ )
$\Delta\varepsilon_{\text{tot}}/2$	$4.88 \times 10^{-4}$	$3.49 \times 10^{-4}$	$7.27 \times 10^{-4}$
$\Delta\varepsilon_{\text{pl}}/2$	$6.1 \times 10^{-6}$	$3.6 \times 10^{-6}$	$2.1 \times 10^{-5}$
$\Delta\sigma/2$	63 MPa	45 MPa	93 MPa

*How does  $\Delta K_{th}$  correlate with  $\Delta\sigma_o$ ?*  
*→ Fracture Mechanical Measurements*

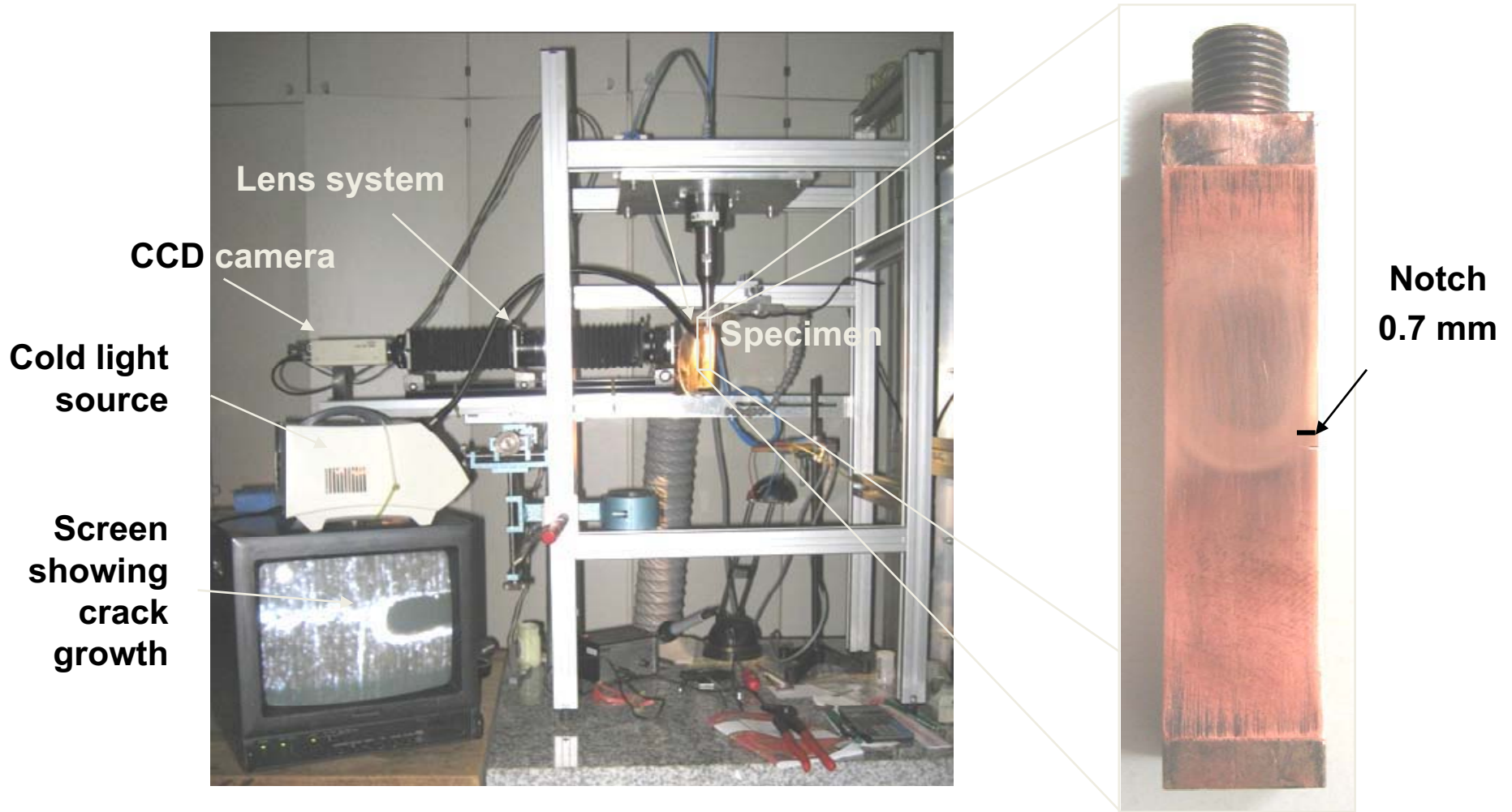


*Torino*  
*5 novembre 2008*

*Stefanie Stanzl-Tschegg*



# Measurement of Crack Propagation



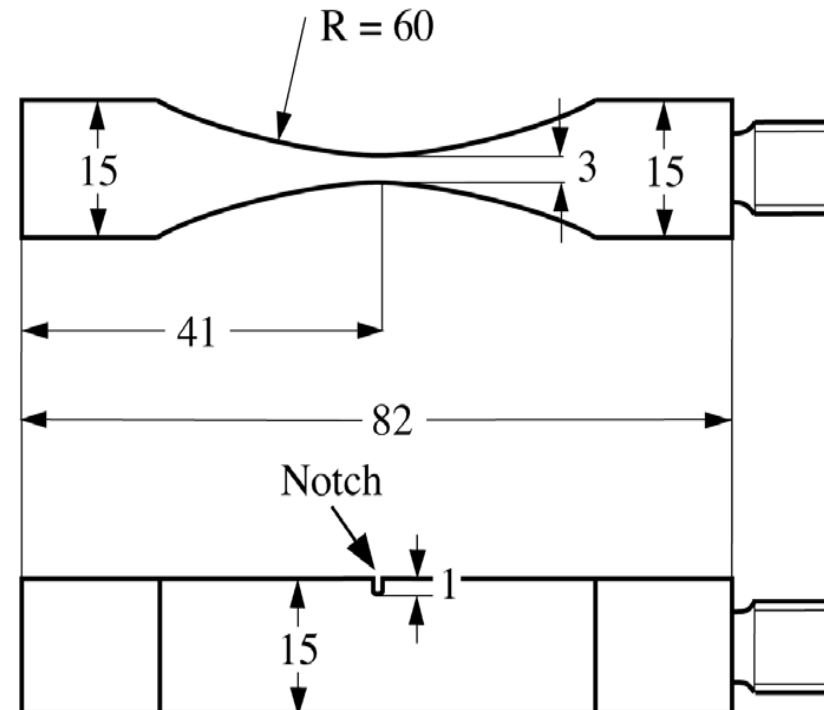
Measurement set-up

SEN specimen

# Ultrasound Fracture Mechanics

Crack propagation and cyclic stress intensities

Notched specimens

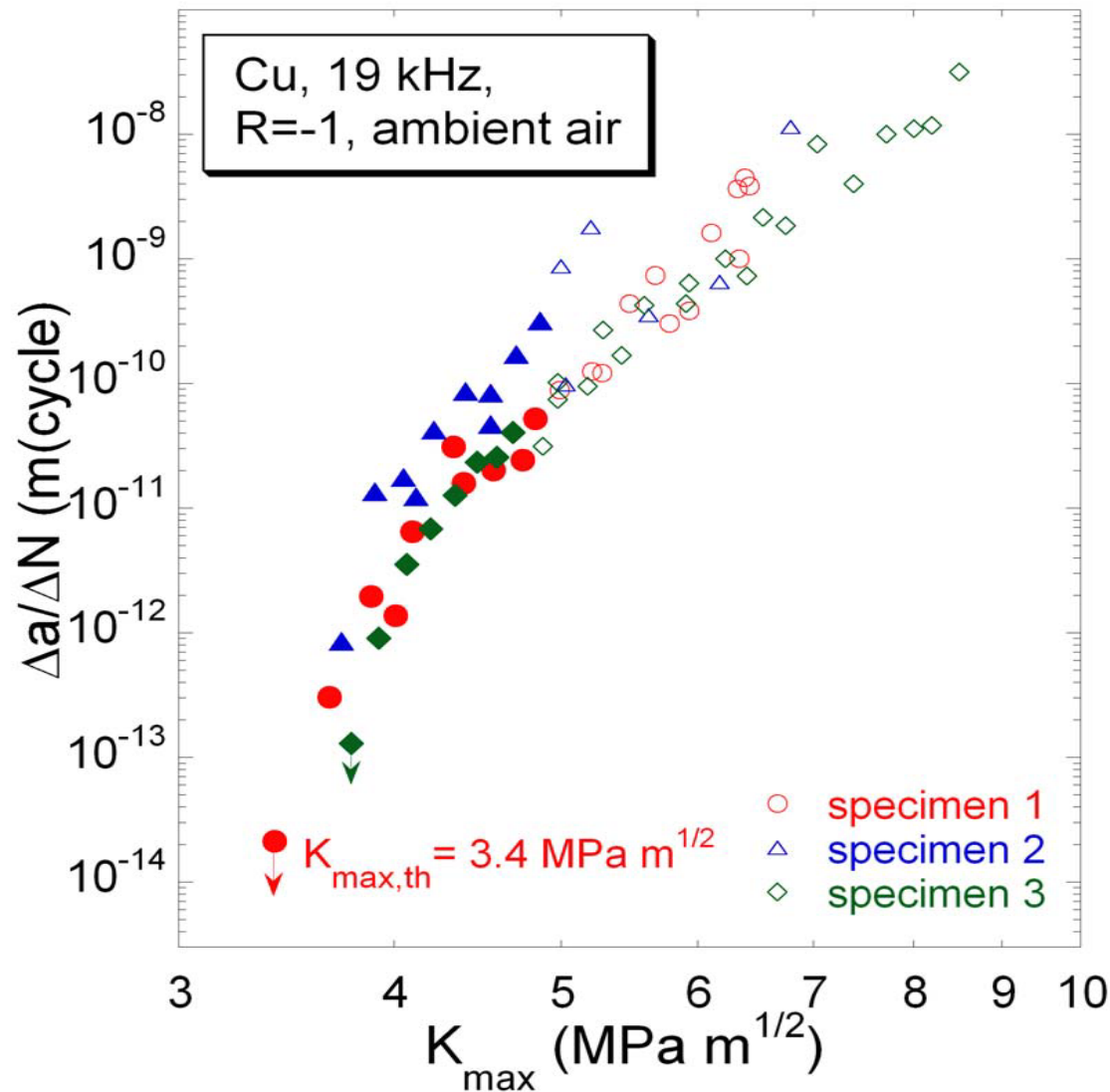


$$K_{\max} = \varepsilon_{\max} \cdot E \cdot \sqrt{\pi a} \cdot Y \left( \frac{a}{W} \right)$$

$$Y = 1.12 - 0.04 \cdot \left( \frac{a}{W} \right) + 0.53 \cdot \left( \frac{a}{W} \right)^2 + 7.8 \cdot \left( \frac{a}{W} \right)^3 - 24.0 \cdot \left( \frac{a}{W} \right)^4$$



# $\Delta a/\Delta N$ vs. $\Delta K/2$ ( $= K_{\max}$ ) Curve



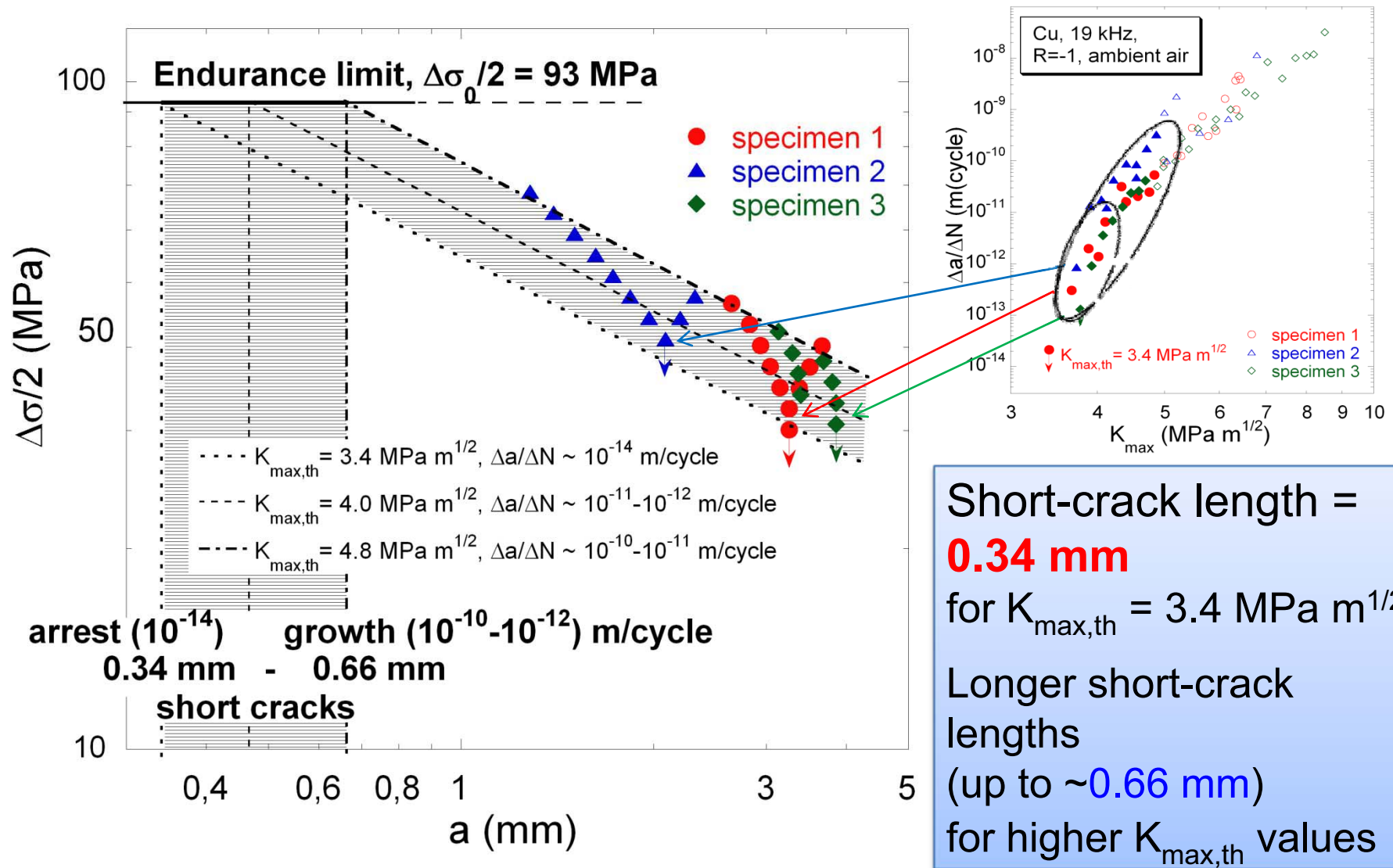
Long crack threshold

$$K_{\max,th} =$$

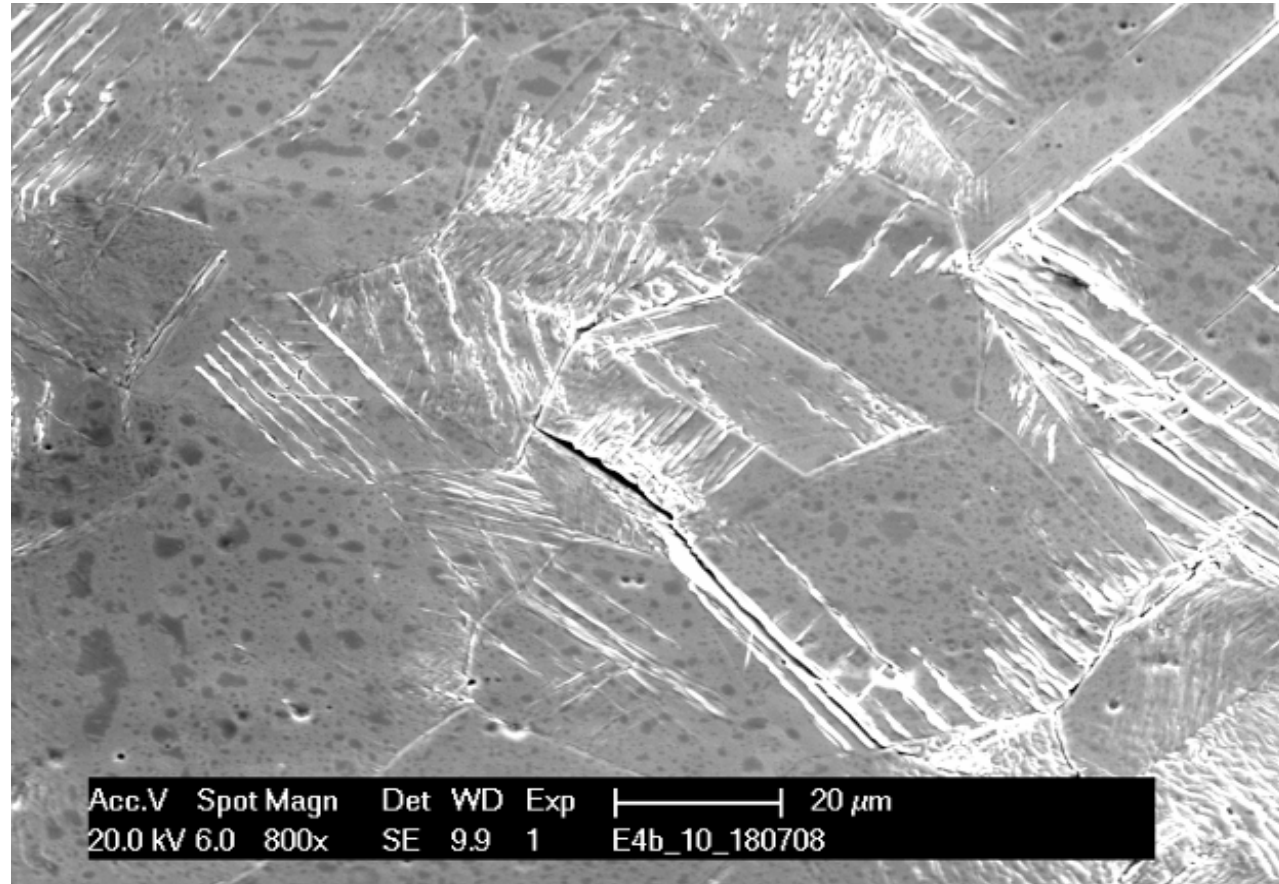
$$3.4 - 4.8 \text{ MPa m}^{1/2}$$

$$\text{for } \Delta a/\Delta N = 10^{-14} - 10^{-10} \text{ m/cycle}$$

# Comparison $\Delta K_0$ - $\Delta\sigma_0/2$ (Kitagawa Diagram)



# Reasons for difference of PSB Threshold and Endurance Limit?



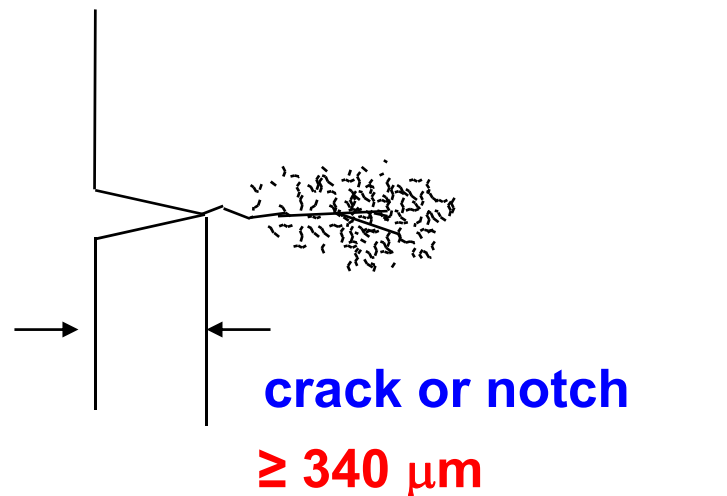
**Numerous small cracks, but *no long crack* below endurance limit ( $\Delta\sigma/2 \sim 87$  MPa)**

# Formation of LONG cracks above endurance limit, but only SMALL cracks below endurance limit

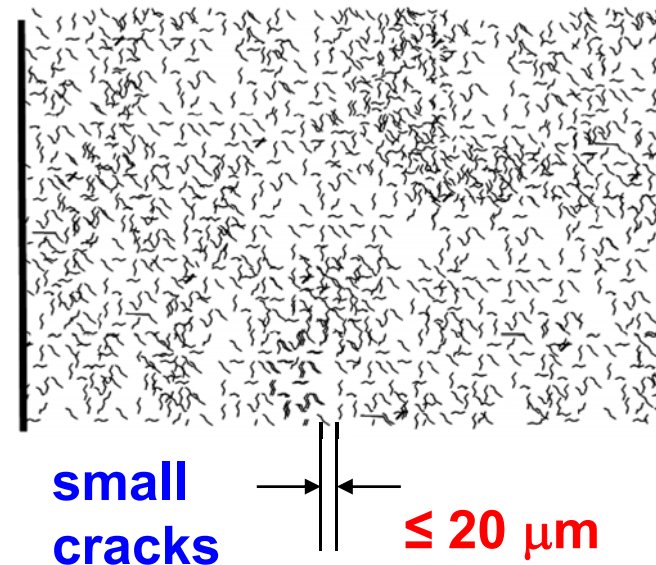
Formation of long propagating cracks (VHCF, 19 kHz)

- at  $\Delta\sigma$  and  $\Delta\varepsilon_{pl}$  values  $\sim 50\%$  above “conventional” PSB threshold
- necessary “short” crack (or notch) length (from Kitagawa diagram)  $\geq 340 \mu\text{m}$
- at “conv.” PSB threshold crack length actually only  $\leq 20 \mu\text{m}$

$\Delta\sigma \geq 93 \text{ MPa}$ :



$\Delta\sigma \leq 63 \text{ MPa}$



# Evolution of Damage (VHCF, 19 kHz)



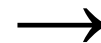
Below endurance limit, above PSB threshold:

**numerous non-propagating small cracks**

→ stress relaxation of loaded volume

Above endurance limit,  $\Delta\sigma$  or  $\Delta K$  high enough for

**long propagating crack**



**failure**

# Summary

- **Ultrasonic fatigue technique** most efficient for VHCF testing.
- **S-N curves** beyond  $10^8$  up to several  $10^{11}$  cycles → question on existence or non-existence of **fatigue limit** may be answered („fish-eye“ fractures...).
- Analogous: ( $\Delta a/\Delta N$  vs.  $\Delta K$ ) **curves** down to  $10^{-14}$  m/cycle → (non)-existence of  $\Delta K_{\text{threshold}}$
- **No frequency effect** for most technical alloys.
- **Frequency influence** for very ductile materials and in corrosive environment **ABOVE**  $\Delta K_{\text{threshold}}$



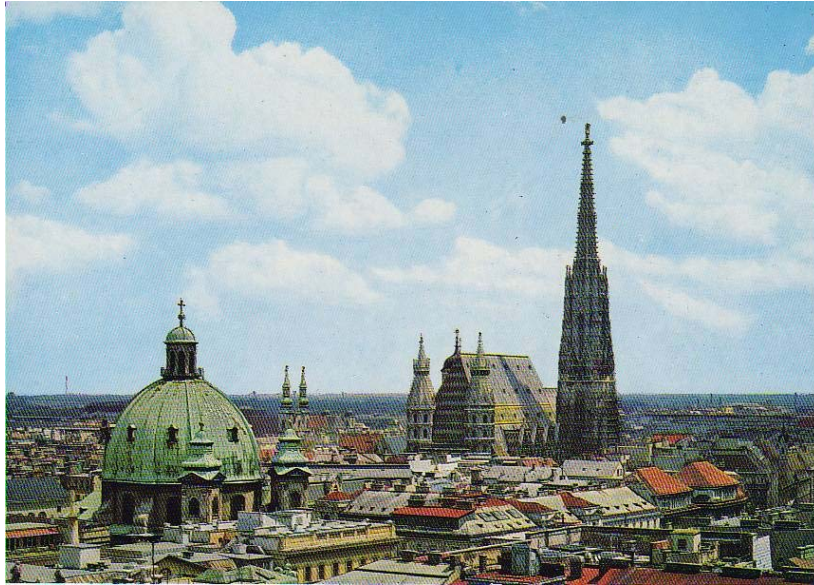
*Torino*  
*5 novembre 2008*

*Stefanie Stanzl-Tschegg*



# Summary

- Tests on **polycrystalline copper**:
- PSBs form below „conventional“ PSB threshold (63 MPa)  
**PSB formation depends on amplitude AND number of cycles** („VHCF threshold“: 45 MPa)
- **Endurance limit** ( $\Delta\sigma_0$ ): Failure at  $\Delta\sigma = 93$  MPa after  **$1.1 \times 10^{10}$  cycles**. No failure below  $\Delta\sigma_0$  within  $2 \times 10^{11}$  cycles.
- **Correlation of  $\Delta K_{th}$ ,  $\Delta\sigma_0$  and relevance of PSB threshold**  
Kitagawa diagram →  
Critical short-crack length is  $\sim 340 \mu\text{m}$  for  $\Delta K_{th}$   
**At/below PSB threshold**: actual crack length  $\sim 20 \mu\text{m}$  →  
No long crack propagation → **no failure**



*Thanks for  
your  
attention!*



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5 novembre 2008

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