

TESTING OF CRACKING SENSITIVE MATERIALS BY THE METHOD OF X-RAY FRACTOGRAPHIC

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The study of failure toughness (K_{IC}) and evaluation of plastic deformation zones in the fractures of structural steels of different strength levels ($\sigma_{0.2} = 256 \dots 1050$ MPa) allowed to establish the correlation between K_{IC} and the size of prefailure microzone h_A [1]:

$$K_{IC} = [\pi(2h_A) \sigma_{0.2} E (1-\nu^2)^{-1} \ln(1-\psi)^{-1}]^{1/2} \quad (1)$$

where: $\sigma_{0.2}$ - yield strength; E - Young's modulus;
 ν - Poisson's ratio; ψ - sample cross-sectional area contraction ratio.

In microzone h_A the microzone of failure (the nuclei of the crack with radius r_* with deformation energy critical density W_C) being formed, K_{IC} and r_* can be correlated as follows:

$$K_{IC} = [r_* W_C 2\pi E / (1+\nu)(1-2\nu)]^{1/2} \quad (2)$$

where W_C is for specific failure work [2].
 From the equations (1) and (2):

$$r_* / h_A = \sigma_{0.2} (1-2\nu) \ln(1-\psi)^{-1} / W_C (1-\nu) \quad (3)$$

Assuming that brittle failure $\sigma_{0.2} \approx S_k$ (where S_k is the real rupture stress), $\psi_{\min} \approx 0.001$ and accounting (3) we can find r_*^{\min} , and from equation (1) - the minimum value $K_{IC}^{\min} = K_{IC0}$, corresponding to the limit embrittlement of the material, when the plastic deformation energy in zone h_A , comparable with the value of structural parameter - can be neglected.

As:

$$W_C = (1+\nu)(1-2\nu) \sigma_{y*}^2 / 2E \quad (4)$$

jointly solving equations (2) and (4), we get:

$$K_{IC} = \sigma_{y*} \sqrt{\pi r_*} \quad (5)$$

or:

$$K_{IC} = \sigma_{y*} \sqrt{\pi r_*^{\min}} \quad (6)$$

where: σ_{y*} - stress σ_y at the distance r_* from the crack tip.

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The calculations based on equations (1 ... 5) with an account of experimental values h_A , S_K , E , ν and W_C showed that for steels the value of G_{y*} varies insignificantly and equals (0,115 ... 0.135) E.

The knowledge of K_{IC0} allows to define the minimum critical size of defect (crack) and to estimate the value of energy intended for the formation of plastic deformation zone (K_{IE}^{ti}) in material in question at given temperature (t_i).

$$\begin{aligned} K_{IE}^{ti} &= K_{IC}^{ti} - K_{IC0} \\ K_{IE}^{max} &= K_{IC}^{max} - K_{IC0} \end{aligned} \quad (7)$$

The brittle failure giving: $K_{IC0} = K_{IC} = K_{IC}^{max}$ and $K_{IE}^{min} \cong 0$, and quasibrittle and ductile failure giving: $K_{IC0} < K_{IC}^{ti} < K_{IC}^{max}$ and $0 < K_{IE}^{ti} \leq K_{IE}^{max}$ the difference $K_{IE}^{max} = K_{IC}^{max} - K_{IC0}$ characterises the maximum plastic deformation energy in material with crack.

Nondimensional value of $k_{IE}^{ti} = K_{IE}^{ti} / K_{IE}^{max}$ can be taken as failure toughness safety factor at a given temperature t_i . In the tough-brittle transition temperature interval k_{IE}^{ti} can vary within the range: $0 \leq k_{IE} \leq 1$.

REFERENCES

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