Cyclic Elasto-Plastic Fracture Diagram as Applied to a Specimen with Crack

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Abstract. This Analytical and experimental method for the estimation of crack growth resistance under cyclic elasto-plastic deformation based on measuring of local plastic strain near the crack tip and is proposed. Diagram of cyclic elasto-plastic fracture of a specimen with crack is constructed as an integral characteristic in terms of nonlinear fracture mechanics. This diagram is the dependence between stress intensity factor determined with the account of plasticity and transverse component of residual strain. A set of cyclic crack growth resistance parameters of plastic steel is determined according to this diagram.

Introduction

Analytical and experimental method for the estimation of crack growth resistance under cyclic elasto-plastic deformation based on measuring of local plastic strain near the crack tip and is proposed.

Diagram Construction Method. The section headings are in boldface capital and lowercase letters. Considering that plastic steel was subjected to test an estimation of applicability of basic formulas of linear elastic fracture mechanics was made. Observance of flat deformation conditions was checked by criteria [1- 4]:

$$K_I \le K_I^* = \sqrt{t_0 \sigma_{0,2}^2 / 2{,}5}; \tag{1}$$

$$\psi = \frac{t_0 - t_\varphi}{t_0} \cdot 100\ \% \le 1{,}5\ \%. \tag{2}$$

where K_I is stress intensity factor (SIF); t_0 is a nominal thickness of the compact specimen; t_φ is a thickness of the compact specimen with the account of elasto-plastic strains; $\sigma_{0,2}$ is yield strength (offset = 0.2%) of a material; ψ is relative contraction of cross-section of the specimen (Fig. 1).

It has appeared that conditions Eq. (1) and Eq. (2) are not satisfied for the investigated steel in the upper part of the fatigue crack growth diagram. Formulas of linear elastic fracture mechanics for the estimation of SIF value of the standard compact tension specimen [1-3]

$$K_{I\,\max} = \frac{P_{\max}\sqrt{l}}{t_0 B} \cdot Y\left(\frac{l}{B}\right), \tag{3}$$

where $P_{\max}$ is the maximum load of a cycle; l is the measured length of a crack; t_0, B are the sizes of a dangerous section of the specimen (Fig. 1); $Y\ (l\ /\ B)$ is the correction function which considers geometry of the specimen and its scheme of loading:

$$Y(l/B) = 29{,}6 - 185{,}5(l/B) + 655{,}7(l/B)^2 - 1017(l/B)^3 + 638{,}9(l/B)^4, \qquad (4)$$

is also correct for elastic deformation under preservation of flat deformation conditions. In order to apply them to elasto-plastic domain it is necessary to correct them for plasticity.

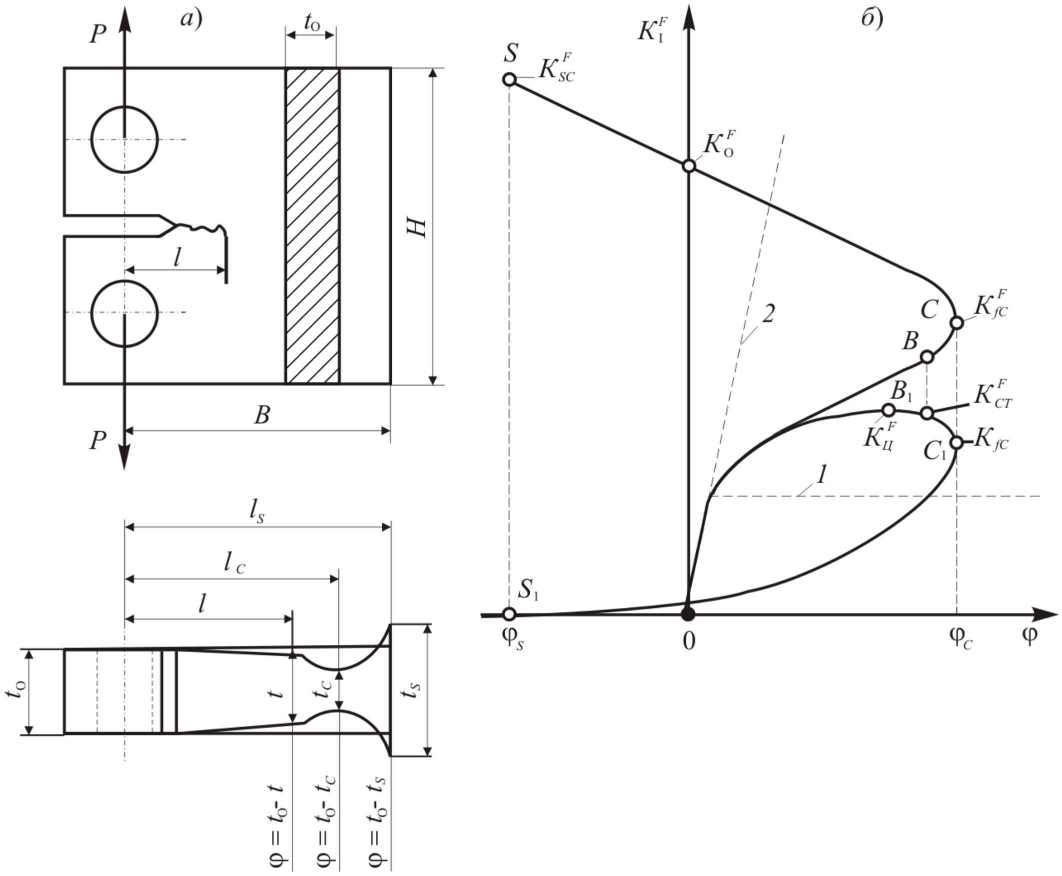

Fig. 1. Schemes: test of the compact specimen and measurement of the thickness reduction (*a*); cyclic elasto-plastic fracture diagram for a specimen with a crack (*b*)

It can be realized by taking into account in Eq. (4) the actual sizes of dangerous cross-section of the specimen, i.e. those sizes that take place under plastic deformation [5 - 9].

Let us multiply and divide the relation l / B by t_0 value; thus $l / B = (l / B)\,(t_\varphi / t_0)$. Means, $Y(l / B) = Y[(l / B)(t_\varphi / t_0)]$. At elastic deformation this equality is identical. Taking into account plastic deformation of dangerous cross-section of the specimen in function Y it is necessary to accept the actual thickness $t_\varphi = t_0 - \varphi$ of the specimen, where φ is a lateral component of plastic strain (contraction) of cross-section, i.e. we can write [5]:

$$Y\left(\frac{l}{B}\,\frac{t_\varphi}{t_0}\right) = Y\left(\frac{F_l}{F_0}\right) = Y(\omega_F), \qquad (5)$$

where F_0 is the nominal (before deformation) area of dangerous cross-section of the specimen; F_l is the area damaged by a crack with a length l and defined with the account of the plastic deformation of cross-section. It means that by introduction of Eq. (5) into Eq. (3) and Eq. (4) we obtain a technique of SIF calculation for elasto-plastic domain [5 - 9]:

$$K_{I\,\max}^F = \frac{P_{\max}}{t_0\sqrt{B}}\,\omega_F^{1/2}\,Y(\omega_F)\,; \qquad (3a)$$

$$Y(\omega_F) = 29{,}6 - 185{,}5(\omega_F) + 655{,}7(\omega_F)^2 - 1017(\omega_F)^3 + 638{,}9(\omega_F)^4. \quad (4a)$$

Thus Eq. (4a) considers not only geometry of the specimen and its scheme of loading but also integrally the size of plastic strain in dangerous cross-section. And in Eq. (3a) the local measure of damage of a specimen with a crack $\omega_F = F_1 / F_0$ that has not only geometrical meaning but also physical content is introduced. This measure unambiguously defines the life of an object with a crack [10]. It should also be stressed out that the measure ω_F is defined taking into account plastic strain of dangerous cross-section.

According to the developed approach [5 - 9] whole process of elasto-plastic deformation and destruction are described by means of the cyclic elasto-plastic fracture diagram for a specimen with a crack (CEPF-diagram). This diagram is built in SIF coordinates K_I^F and absolute φ or relative ψ contraction. Lateral component of plastic strain of the specimen in the zone of crack growth (contraction) is defined as a difference between nominal t_0 and actual t_φ values of thickness of the specimen, i.e. $\varphi = t_0 - t_\varphi$ (see Fig. 1,a); its relative value is $\psi = \varphi / t_0$. Thus SIF K_I^F is calculated using formulas of linear elastic fracture mechanics, but adjusted for plasticity of the investigated material. For example Eq. (3a), (4a) are used for calculation of SIF of the compact specimen (see Fig. 1,a).

Two types of CEPF-diagram. There are two types of CEPF-diagram [7-9]. If for calculation of K_I^F value we conditionally accept that the maximum load in rupture process remains constant (and it is really possible if the test machine is rigid enough or loading rate is high), then *OBCS* diagram (see Fig. 1, *b*) is obtained which resembles letter *D* taking into account ordinates axis. Therefore it is named *D*-diagram. If for calculation of K_I^F we consider decrease of loading in rupture process of a specimen (when the test machine has rather low rigidity or the rate of loading is low) diagram $OB_1C_1S_1$ (see Fig. 1, *b*) is obtained. As the form of this diagram reminds letter *Q* it is named *Q*-diagram.

The CEPF-diagram generally consists of two curves: a curve of cyclic elasto-plastic destruction (sections *OBC* in *D*-diagram and OB_1C_1 in *Q*-diagram) and a curve of quasi-static destruction (rupture) (sections *CS* in *D*-diagram and C_1S_1 in *Q*-diagram). In points *C* and C_1 the crack reaches the critical size l_c to which limiting contraction φ_c and limiting SIF value - cyclic fracture toughness (values of K_{fc}^F in *D*-diagram and K_{fc}^* in *Q*-diagram) correspond. There is a division of the specimen into two parts in corresponding points *S* and S_1 , thus takes place a maximum limiting widening φ_s it's dangerous cross-section on which we define other limiting SIF value - the quasi-static fracture toughness (size K_{sc}^F in the *D*-diagram; $K_I^F = 0$ in this point in *Q*-diagram). Crossing of *CS* curve with an axis of ordinates gives one more parameter of crack growth resistance K_0^F (see Fig. 1, *b*). The maximum of *Q*-diagram on an SIF axis (point B_1) corresponds to the beginning of cyclic rupture and is characterized by parameter $K_{\text{ц}}^F$; parameter $K_{\text{ст}}^F$ in the *Q*-diagram corresponds to the beginning of quasi-static rupture; it is not a characteristic point of this diagram, but it corresponds to the beginning of sharp lifting of curve *OBC* (a point *B* in the *D*-diagram). In a case of "ideally plastic fracture" the curve of cyclic elasto-plastic destruction is transformed to a straight line 1. In a case of "ideally brittle fracture" (φ = 0) this curve coincides with an axis of ordinates. The line 2 divides areas of quasi-brittle and elasto-plastic destructions. Thus the analysis of is viscous- brittle transition, for example, at change of the sizes of a specimen or test temperature is possible by means of CEPF-diagram.

Parameters of CEPF-diagram. It is offered three expressions for the analytical description of *OBC* curve at *D*-diagram [5, 7-9]. The first is a power equation

$$K_I^F = K_{th}^{\varphi} \cdot \varphi^{m_1} \tag{6}$$

where m_1 is a parameter of cyclic hardening ($0 \le m_1 \le 1$); K_{th}^{φ} is a plasticity threshold, i.e. SIF value below which the plastic strains in a crack top do not influence its value. Parameters m_1 and K_{th}^{φ} are defined on experimental dependence in co-ordinates $\lg K_{\mathrm{I}max}^F - \lg(\varphi/\varphi_{th})$.

The second dependence for the description of a curve of cyclic elasto-plastic destruction *OBC* looks like:

$$K_I^F = K_w \left(\frac{\psi - \psi_t}{\psi_c - \psi} \right)^{m_2} \quad \text{if} \quad \psi_t < \psi < \psi_c, \tag{7}$$

where K_w is the parameter which is subject to definition; m_2 is parameter of hardening; ψ_t is a relative contraction of a specimen, corresponding to the beginning of yield of a material at an axial tension. If $K_I^F = K_w$, $2\psi = \psi_c + \psi_t$ or $\psi = (\psi_c + \psi_t) / 2$. Hence parameter K_w is such SIF value which corresponds to relative size of contraction $\psi = (\psi_c + \psi_t) / 2$. And as $\psi_t \to 0$ and for plastic materials $\psi_c >> \psi_t$ so parameter K_w can be defined for them as such value K_I^F which corresponds to half of limiting contraction ($\psi_c / 2$). Practically value K_w is defined also as value corresponding to value *lg* $[(\psi - \psi_t) / (\psi_c - \psi)] = 0$ at representation of *OBC* curve (see Fig. 1, *b*) in co-ordinates *lg* K_I^F - *lg* $[(\psi - \psi_t) / (\psi_c - \psi)]$, and value of parameter m_2 can be found from the same graph as a tangent of a angle of an inclination of the received straight line to an axis of abscises.

For obtaining the third expression it is accepted that experimental points in an average part of *OBC* part of the *D*-diagram are approximated by a straight line in co-ordinates *lg* K_I^F - *lg* (ψ / ψ_t). The equation of this straight line at transition to usual co-ordinates is transformed to power dependence of a kind

$$K_I^F = K_t \left(\frac{\psi}{\psi_t} \right)^{m_3} \tag{8}$$

where K_t, m_3 are parameters. Practically value K_t is defined on a point of crossing of the specified straight line with an axis of ordinates in double logarithmic co-ordinates, and value of parameter m_3 is found as a tangent of an angle of an inclination of this straight line to an axis of abscises.

Fig. 2 shows CEPF-diagrams (analytical description of which was given above) for compact specimens of different thickness made of the plastic carbonic steel. Influence of specimen sizes on deformation characteristics of crack growth resistance is visible on Fig. 2. And in Fig. 3 the same diagrams are combined in the form of one dependence SIF-specimen contraction by means of the offered similarity transformation. It is shown how the stated approach can be used for an estimation of pipes survivability.

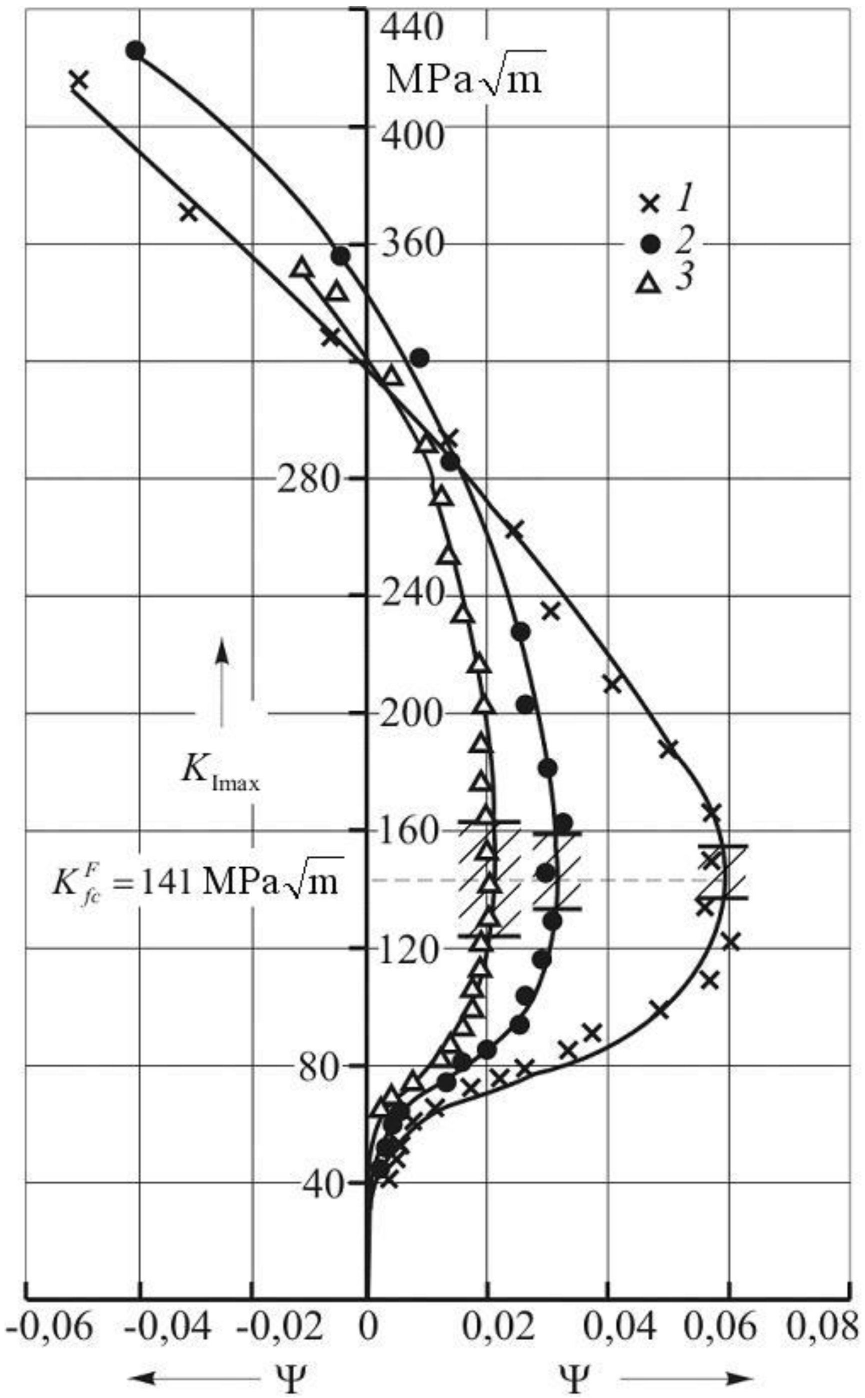

Fig. 2. CEPF-diagrams for the carbonic steel constructed by the results of tests for compact specimens of 10 (1), 20 (2) and 40 (3) mm thickness

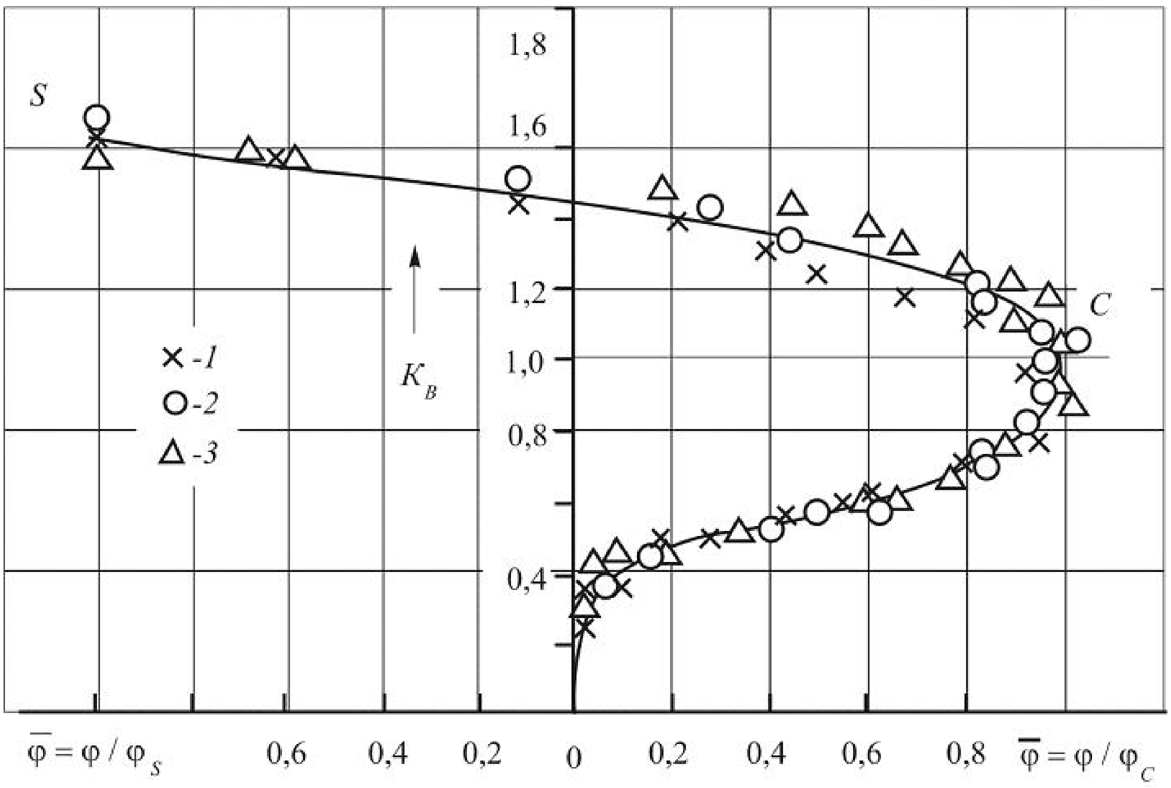

Fig. 3. Generalized CEPF-diagrams for the carbonic steel constructed by the results of tests for compact specimens of 10 (1), 20 (2) and 40 (3) mm thickness

References

[1] D.M. Maric, P.F. Meier and S.K. Estreicher: Mater. Sci. Forum Vol. 83-87 (1992), p. 119

[1] E-647-00 Standard Test Method for Measurement of Fatigue Crack Growth Rates.

[2] Standard test method for plane-strain fracture toughness of materials, Annual Book of ASTM Standards (E.339-74) (1976) p. 471–490.

[3] РД 50-345-82. Calculations and tests for strength. Methods of mechanical tests of metals. Definition of crack growth resistance characteristics (viscosity of destruction) at cyclic loading. Methodical instructions. Moscow, 1982.

[4] B.A. Drozdovsky and E.M. Morozov, Methods of an estimation of viscosity of destruction, J. Zavodskaya laboratoriya (8) (1976), p. 916-1004.

[5] L.A. Sosnovskiy, Cyclic elasto-plastic fracture diagram for a specimen with a crack and its basic points, J. Vesty AS BSSR, series of phis.-tech. sciences (2) (1990), p. 3-7.

[6] L.A. Sosnovskiy, L.A. Hamaza and N.K. Babich, Experimental research of cyclic crack growth resistance of 0,2% carbon steel, J. Problems of strength (6) (1990), p. 34-38.

[7] L.A. Sosnovskiy and A.V. Bogdanovich, The analysis of a cyclic elasto-plastic fracture diagram for a specimen with a crack. Part 1, J. Problems of strength (5-6) (1995), p. 39-51.

[8] L.A. Sosnovskiy and A.V. Bogdanovich, The analysis of a cyclic elasto-plastic fracture diagram for a specimen with a crack. Part 2, J. Problems of strength (5-6) (1995), p. 52-61.

[9] L.A. Sosnovskiy and A.V. Bogdanovich, Crack Resistance, BelSUT, Gomel, (2011), 366 p.

[10] L.A. Sosnovskiy, Statistical mechanics of fatigue fracture, Science and Technics, Minsk, (1987), 288 p.